

Universitat Autònoma de Barcelona

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### -TECHNICAL NOTE 25.2-

### PHOTOSYNTHETIC PILOT REACTOR

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### 1. Introduction.

The MELISSA Pilot Plant, currently located at the Department of Chemical Engineering of the Universitat Autònoma de Barcelona, has been conceived to integrate the knowledge developed by the different groups involved in the project, and to demonstrate the feasibility of the concept and the robustness of its operation. At the present time, two bioreactors, corresponding to compartments III an IV of the MELISSA loop (as described in Figure 1), are in operation in the Pilot Plant. The bioreactor corresponding to compartment IV, where the cyanobacteria Spirulina platensis is grown using the light as energy source, is the most developed so far. As a step forward in the development of the Pilot Plant, the second phase of the work plan, includes the design and construction of a new bioreactor for compartment IV. Simultaneously, the bioreactor currently used for Spirulina will be modified to adapt it to the culture of Rhodobacter cells for compartment II (a proposal for these modifications is presented in TN 25.4). In this TN a basic proposal regarding the concept for the new bioreactor is made. In case of acceptance by ESTEC, this proposal will be discussed with the bioreactor manufacturer to establish all the specific details in order to proceed to its construction and set-up. Three main aspects constitute the driving force for the new bioreactor design :

- to scale-up the volume of the bioreactor to a volume enabling a oxygen production to sustain the life of three rats.

- to maintain as far as possible the current type of bioreactor, in order to use efficiently all the knowledge developed in the present unit (for example, the knowledge model between cell growth and light intensity).

- to improve the operation of the bioreactor proposing alternatives for some of the peripheral equipment/instrumentation. Some of these changes are due to the availability of new equipment, and others are directly linked to the change of size. The number of changes should be minimised to those with a clear impact in the reactor operation. According to these objectives, this TN has been divided in two parts : new bioreactor design and auxiliary equipment. A detailed description of the bioreactor currently employed has not been considered necessary, as can be easily obtained from

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**Figure 1.** General concept of MELISSA and its compartments. previous MELISSA documentation (Binois 1994).

### 2. The new bioreactor design.

### 2.1 Basic considerations

As mentioned in the introduction, two previous requirements for the design are to use the same concept of bioreactor, that is, an air-lift, and to scale-up the working volume to be able to sustain the life of three rats. In order to scale-up the current bioreactor to its new size several preliminary points were considered :

- the size increase could require an increase in the reactor diameter. This would reduce the ratio of surface to volume in the reactor, therefore making more difficult the illumination of the cells. Qualitatively, given a cell concentration, for the same intensity of the light at the external surface of the reactor (Fr), the light intensity in the centre of the bioreactor will be lower for a larger diameter. This will generate, especially when high concentrations of cells would be desired, a dark volume inside the bioreactor, in which the light intensity would be too low (<1W/m<sup>2</sup>) and where the

cells would not grow. This drawback of a diameter increase could be compensated by increasing the Fr. However this has a physical limit (the level of Fr required for a large diameter may not be attainable), and, more important, too high Fr would cause inhibition to the cells growth. Thus, increasing Fr from 400 W/m<sup>2</sup> would possibly create a volume of the reactor where cell growth would be inhibited.

- the scale-up in the reactor volume can not be realised only by maintaining the diameter of the present bioreactor and increasing its height, because the height of the laboratory imposes obvious restrictions. In addition, the construction and the working conditions (for example pressure) would also be more adverse.

-in terms of reactor homogeneity regarding illumination, a desirable feature of the design is to have a high ratio between the volume of the illuminated zone with respect to the total reactor volume (Vil/Vt). This ratio is 0.52 for the reactor presently used.

- a meaningful magnitude to calculate in the design of the reactor is the volumetric rate of energy absorbed in the photobioreactor,  $\langle A \rangle$ , which is related to the radiant energy available and therefore to cell growth rate. As described by Cornet et al (Cornet et al, 1993), the relationship between Fr and  $\langle A \rangle$  for a cylindrical reactor is given by

$$\frac{A}{2F_r/R} = \frac{2 \cdot \alpha \cdot \sinh \cdot \delta R}{\cosh \delta R + \alpha \cdot \sinh \delta R}$$
(1)

As  $\langle A \rangle$  depends of the way to illuminate the reactor and its geometry, it is a specific data of a bioreactor. However, when the mono-dimensional approximation is expected, equation (1) will remain valid as long as the cylindrical geometry is not changed. Therefore, this relationship can be used to study what increase in Fr is required to maintain the same values of  $\langle A \rangle$  in reactors with different diameters.

Taking into account these different aspects, some alternatives for the bioreactor design have been studied, and their main features are summarised below. In order to do some of the calculations, basically those linking the incident radiant energy flux at the external surface of the bioreactor (Fr) and the radiant energy flux at the centre of

the bioreactor (Eb) the corresponding sections of the PHOTOSIM program have been used.

The four configurations used to study the effects of the design on the different magnitudes of the reactor are :

- the air-lift reactor presently used (reactor 1, figure 2)

- an air-lift reactor with an increased diameter of 0.12 m (reactor 2, figure 3)

- an air-lift reactor with an increased diameter of 0.17 m (reactor 3, figure 4)

- an air-lift reactor with an external loop, with a diameter of 0.12 m (reactor 4, figure 5)



Figure 2. Current air-lift bioreactor configuration (reactor 1).

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Figure 5. External loop air-lift configuration (reactor 4).

In all the bioreactors proposed, the different design relationships, such as the ratio between reactor and internal draft tube diameter, or the ratio between the reactor diameter and the gas separation section have been calculated according to the general criteria proposed in the literature of air-lift bioreactors (Chisti 1989, Chisti and Young 1993).

Table 1 gives the values of the different radius according to the scheme proposed in figure 6 and the mathematical model developed previously (Cornet et al. 1993), employed for each reactor in the simulations done with PHOTOSIM.

	reactor 1	reactors 2,4	reactor 3
R	0,048	0,06	0,085
r1	0,0302	0,0497	0,068
r2	0,02585	0,0447	0,063
r3	0,0115	0,0115	0,0115
rb	0,0095	0,0095	0,0095

 Table 1. Values of the different radius corresponding to the reactors studied, according to Figure 6, as used in PHOTOSIM.



Figure 6. Definition of the different radius in the reactor.

Table 2 gives the values of some general magnitudes for each reactor. It can be observed that the ratio between the illuminated area to the total reactor volume is maintained at similar level for most of the designs, with a considerable increase for configuration 2. For that case, the ratio of the illuminated to total volume is also highest. However, this configuration is not possible, because the height is too high. This, in addition to the limitations of the pilot plant laboratory would add difficulties in the construction and operation of the reactor.

Regarding the illumination conditions, the results obtained with PHOTOSIM for the current bioreactor (diameter 9.6 cm) and the two diameters used as study case (12 and 17 cm) in this TN, using different criteria, are summarised in tables 3 to 6.

	reactor 1	reactor 2	reactor 3	reactor 4
Useful volume (dm <sup>3</sup> )	7	49,97	49,96	54
Illuminated volume (dm <sup>3</sup> )	3.68	42,95	38,56	37,3
Illuminated volume/total volume	0,52	0,85	0,77	0,69
Illuminated area/total volume (m <sup>-1</sup> )	21,54	28,64	18,16	22,9

Table 2. Values of some general magnitudes for the different reactors studied

In table 3, the Eb values at the centre of the current bioreactor are calculated for two different values for Fr (195 and 400 W/m<sup>2</sup>) and Cx (0.7 and 1.4 g/l). This conditions are taken as a basis for the comparison of the simulation results of the different configurations. It should be noticed that in this case, for the higher cell concentration the corresponding Eb values are below the value limiting cell growth (1  $W/m^2$ ).

In table 4, the Eb values for the same situations studied in table 3 are given for the other two diameters, 12 and 17 cm. The drastic effect of the diameter on the light availability is evident, and these results corroborate quantitatively the limitation of the scale-up procedure regarding diameter increase. This fact can also be observed in the results presented in tables 5 and 6.

In table 5, the values of Fr necessary for the two new diameters in order to maintain the same  $\langle A \rangle$  values than for the current configuration, and their corresponding Eb, are given. It can be noticed that in spite of the increase in Fr to values higher than 400 W/m<sup>2</sup>, the Eb values are very low for the case of 17 cm

diameter, and about 10% for 12 cm diameter, when compared to the data in Table 3.

Table 6 gives the results when the calculations are made using the criteria of obtaining the same Eb value for the 12 and 17 cm configurations, than in the current configuration, for the conditions in table 3. In accordance to the previous points it can be observed the high Fr values that should be required.

Fr	Cx	Eb	<a></a>
195	0,7	25,07	7768,9
195	1,4	0,356	7768,9
400	0,7	51,42	15807
400	1,4	0,73	15807

Table 3. Eb values for reactor 1 at different conditions.

<a></a>	Cx	Fr	Fr	Eb	Eb
		reactors 2,4	reactor 3	reactors 2,4	reactor 3
7768,9	0,7	241,8	342,5	8,52	0,604
7768,9	1,4	241,8	342,5	0,026	6,64E-05
15807	0,7	495,94	702,6	17,478	1,239
15807	1,4	495,94	702,6	0,054	1,36E-04

**Table 4.** Eb and <A> values for the different configurations, for the same conditions used in table 3.

Fr	Cx	Eb	<a></a>	Eb	<a></a>	Eb	<a></a>
		reactor 1	reactor 1	reactors 2,4	reactors 2,4	reactor 3	reactor 3
195	0,7	25,07	7768,9	6,872	6215	0,344	4387
195	1,4	0,356	7768,9	0,021	6215	3,78 E-5	4387
400	0,7	51,42	15807	14,097	12749	0,705	8999
400	1,4	0,73	15807	0,044	12749	7,759 E-5	8999

**Table 5.** Values of Fr and Eb for the different configurations, for the same <A>values than reactor 1.

Eb	Cx	Fr	Fr
		reactors 2,4	reactor 3
25,07	0,7	711,3	1,42E+04
0,356	1,4	3,24E+03	1,83E+06
51,42	0,7	1,46E+03	2,92E+04
0,73	1,4	6,65E+03	3,76E+06

Table 6. Values of Fr for the different configurations, for the same Eb than reactor 1.

In conclusion, from the results of these calculations, and taking into account the rest of criteria already enumerated, the basic concept proposed for the new *Spirulina* bioreactor is as configuration 4. That is, an air-lift bioreactor with an external loop downcomer, and with a relatively moderate increase in diameter (new diameter around 12 cm) with respect to the current configuration. This design represents a compromise between volume required, physical size, illumination conditions, and relatively simple configuration.

Following this conclusion, a more detailed design of the bioreactor has been elaborated. For this the volume and illumination needed to fulfil the preliminary requirement of sustaining the life of three rats has been taken into account.

### 2.1 Bioreactor sizing and detailed design.

According to the previous results obtained with rats (de Chambure 1992, Tranquille 1992) it will be assumed that a rat (weighing between 200-400 g) can consume 25 g/day of *Spirulina*. This rats consume about  $11 \text{ O}_2/\text{Kg} \cdot \text{h}$  and evolve  $0.91 \text{ CO}_2/\text{kg} \cdot \text{h}$ . Therefore for an hypothetical experiment using 3 resting rats of about 400 g in weight, 3.125 g/h of *Spirulina* have to be produced. At the same time this *Spirulina* should produce at least  $1.21 \text{ O}_2/\text{h}$  ( $5.36 \text{ 10}^{-2} \text{ mol O}_2/\text{h}$ ) and consume about  $1.081 \text{ CO}_2/\text{h}$ . If the rats are in an active state a coefficient of 2.5 can be applied to correct for the increased oxygen consumption. This results in a consumption of a  $31 \text{ O}_2/\text{h}$  ( $0.134 \text{ mol O}_2/\text{h}$ ) and an approximate production of  $2.71 \text{ CO}_2/\text{h}$ . Those values have been taken as a starting point for the following calculations.

Using PHOTOSIM, which at this moment can appropriately represent the available experimental data, a bioreactor illuminated with an Fr of 300 W/m<sup>2</sup>, can produce a biomass productivity of 6.9  $10^{-2}$  g · l<sup>-1</sup> · h<sup>-1</sup>. while producing 3.33  $10^{-3}$  mol O<sub>2</sub> · l<sup>-1</sup> · h<sup>-1</sup>. From the oxygen amount needed for the three active rats it can be calculated that a volume of a bioreactor (with the same characteristics as the one used in PHOTOSIM) of 40 1 would be required. A similar calculation done for the biomass produced will give that a bioreactor of 44 1 is required. If we take the 40 1 bioreactor a 90% of the rats daily food intake can be fulfilled. This is judged satisfactorily at this moment as the food intake of the rats is expected to be supplemented, in the laboratory ,either by another compartment in the MELISSA loop or by an external supplement.



Figure 7. Final proposed airliftdesign .

To obtain the total useful volume this illuminated volume has to be corrected by a factor taking into account the fact that not all the bioreactor volume will be illuminated. Therefore if we assume that a bioreactor has a 20% of its volume non illuminated, the final volume will be then around 50 l.

Using the actual 71 bioreactor, the productivity of 6.9  $10^{-2}$  g  $\cdot 1^{-1} \cdot h^{-1}$  mentioned above is attained at 300 W/m<sup>2</sup> for an illuminated surface of 0.154 m<sup>2</sup>. This corresponds to a production of 0.483 g/h of *Spirulina*. Therefore the total consumed illumination power is of 46.2 W.

At this point the assumption that the power consumed for a certain productivity is constant can reasonably be done. Therefore from the above mentioned values of 46.2W consumed for a production of 0.483 g/h and the new desired production of 3.12 g/h it follows that an illumination power of 300 W (298.9) will have to be supplied to the new bioreactor. Taking a security factor of 15%, the illumination power to supply to the new bioreactor has to be around 350 W of useful light energy. The bioreactor surface will be illuminated with 300 W/m<sup>2</sup>, therefore it can easily be calculated that to obtain a total of 350 W the illuminated area required for the new bioreactor has to be of  $1.16 \text{ m}^2$ .

In conclusion, a bioreactor of 401 illuminated volume (higher total useful volume, depending on the ratio of illuminated volume vs. total volume), and having an illuminated area of at  $1.16 \text{ m}^2$  with an Fr. of 300 W/m<sup>2</sup>, will be required. From this data and the basic concept design chosen above, the following final design is proposed.

As represented in figure 7, the final design consists of an airlift bioreactor having a rising tube and an external downcomer both having a 12 cm diameter. The length of this tubes, which constitute the illuminated part of the bioreactor is of 1.65 meters. These two tubes are connected by two stainless steel parts that are double jacketed for temperature control (cooling of the bioreactor is necessary to compensate the thermal energy input from the lamps). The total volume of this bioreactor is of 54 litres (table 7) having an illuminated volume of 37.3 l. This value is slightly below to the 40 l calculated before but on the other hand it has a higher illuminated area,  $1.24 \text{ m}^2$ , instead of 1.16. Moreover this bioreactor has 69% of its

total volume illuminated, which represents a significant improvement from the presently used bioreactor which only has a 52% of illuminated volume. This design represents a compromise between the airlift design and the operational specifications. Figure 7 also shows proposed location for the different probes.

	Actual bioreactor	New design
Illuminated volume (I)	3.68	37.3
Illuminated area (m2)	0.154	1.24
Total volume (I)	7	54
Illuminated Vol./Tot. Vol.	0.52	0.69
Illuminated Area/Tot Vol.	21.54	22.9

 Table 7 : Comparison of reference parameters of the new bioreactor and the bioreactor currently in operation.

### 3. Auxiliary equipment.

The event of the construction of a new bioreactor should be used to review the operation of the auxiliary equipment currently used and propose modifications if necessary. In some cases these modifications appear as a consequence of the change in bioreactor scale. As a principle used in this part, the number of modifications should be minimised, and limited to those more important. No modifications are proposed for the equipment working satisfactorily, even that new alternative equipment may be available. In the following the main aspects proposed to review will be addressed.

### 3.1. Illumination system.

The illumination system is clearly a key element in any photobioreactor. In the present *Spirulina* bioreactor, halogen lamps with variable intensity have been used successfully. The possibility to regulate the light intensity has been a key feature in order to develop an automated control system based on the relationship between light availability and cell growth. Also, the spectra of the halogen lamps was shown adequate to the absorption spectra of *Spirulina* cells (Binois 1994). However, halogen lamps present also important drawbacks. One of them is heat dissipation. The heat produced by the lamps is considerable, making necessary the use of external fans and a cooling system in order to maintain the reactor temperature.

As discussed previously a total of 350W will have to be supplied to the new bioreactor. Taking into account an efficiency of the lamps in converting power energy

to light energy of 5% it follows that the total power of the lamps will have to be of about 7000W. If we assume that the same kind of lamps as used before will be used (Sylvania 12V 20W) a total of 350 lamps will be necessary.

### 3.2. Required power supply for the lamps.

As a source of power for the lamps two possible solutions can be mentioned here. As a first possibility an array of variable power supplies can be used. As the maximum voltage that can be applied to the lamps is 12V and a total of 7000W has to be supplied, the needed power supplies have to provide of total of 583 Amps. The power supplies have to be able to sustain a voltage bigger that 12V to account for the difference of potential loss that will be caused by the wiring. From this specifications it is proposed to obtain the power supplies from the same manufacturer that supplied those currently used (Lambda). The biggest variable power supply this manufacturer is able to supply gives 45 Amps at a 15 Volts. Therefore 13 power supplies will be needed to obtain the 583 Amps.

The wiring of each power supply must hold the 45 A with a minimum resistance to minimise the voltage loses. Assuming normal copper wire is used, a 4.5 mm diameter wire will give a decrease in voltage of 0.5 volts in a 5 metres line, which is acceptable.

As a less expensive alternative it is possible to use a voltage regulator directly on the 220V power line. After this, small fixed voltage converters from 220V AC to 12V DC, can be used. This way when the voltage of the 220V line is regulated a variation in the 12V DC line is obtained.

Final decision on the exact system to implement will be decided after conversations maintained with the ESA technical officer and the lamps supplier.

### 3.3. Cooling capacity required.

Once the total amount of power to be applied to the bioreactor has been estimated (7000W), the cooling needs can also be estimated.

Assuming that the lamps to use have an efficiency of 5% it follows that 95% of

the power (6650W) will be dissipated as heat. Assuming that a proper ventilation system (fan) is available around the bioreactor, this amount of heat will be dissipated in the surrounding air and it will have to be removed by the air conditioning system. Those 6650W are equivalent to 5719 calories/h. As the current air conditioning system is able to remove up to 11200 calories/h, it can be assumed that it will be able to handle this increased amount of heat generation.

On the other hand it can be assumed that the remaining 5% (350W) of energy that has been converted into light will be uptake by the Spirulina culture. Although a part of this 5% energy will be fixed into biomass, the main part of it (about 85%) will be dissipated as heat inside the bioreactor. It can be also considered that as a result of the imperfect aeration around the bioreactor some heat can be transferred from the surrounding air, used to cool the lamps, to the bioreactor. Therefore the above mentioned value of 5% for the heat to be removed from the bioreactor has been increased to 15% to take this effect into account.

It will be assumed that in the less favourable scenario, all this energy is dissipated as heat in the liquid culture. Therefore a liquid cooling system has to be supplied to remove this heat. It is proposed to install double jacketed stainless steel walls for the horizontal parts of the reactor. It should be checked that this will provide enough heat exchange area.

Assuming that the bioreactor must have a temperature of 36 °C, and that the cooling liquid will enter the coil tubes at 4 °C and exit with an increase of 10 °C, a mean logarithmic difference of temperature (DTLM) of 26.7 °C can be calculated as the driving force of the heat removal. An overall heat coefficient of 500 W  $\cdot$ m<sup>-2</sup>  $\cdot$  °C can be taken for this system. Assuming that 1050 W of heat energy have to be removed, a surface of 75  $\cdot$ 10<sup>-3</sup> m<sup>2</sup> are needed for the heat exchanger. The surface that can be provided by using a double jacked on the metallic pipes used to connect the two vessel columns is of 150-200  $\cdot$ 10<sup>-3</sup> m<sup>2</sup> so this is the system proposed for temperature control.

### 3.4. Liquid flow: pumping and measurements.

In the current bioreactor used in the MELISSA Pilot Plant, liquid inlet and

outlet streams are provided by peristaltic pumps. Additionally, no flow measurement is installed on-line, and the operator of the reactor has to check its value at least two times every day. Moreover, the diameter of the tubing in the peristaltic pump changes during continuous operation for long periods. The experiments done with this compartment have shown how sensitive the cell behaviour is with respect to the values of the dilution rate. Also, liquid flow-rate is one of the variables to be modified by the bioreactor control through the GPS, in order to maintain a desired productivity level. Therefore, this aspect should be improved in the design of the new bioreactor in order to have a more robust and reliable operation.

A direct consequence of the increase in bioreactor volume is that, for the usual dilution rates ranges, from 0.01 to 0.05 h<sup>-1</sup>, the liquid flow-rates will range between 0.5 and 2.5 l/h. Thus, the pumps selected will have to cover this range of flow-rates. With the aim to propose an alternative to peristaltic pumps, two different types of pumps seem adequate: membrane and gear pumps. Centrifugal pumps have been discarded because they are not so indicated for precise flow-rates, and the values required are too low for the usual range of operation of these pumps. The technical information of two different types of membrane pumps (Alldos M 205 Etron M, 205-3.0/E05, and Prominent gamma/4 G/4a-0703) are given in appendix 2. The technical information of Ismatec gear pumps and Tuthill magnet drive gear pumps is given in appendix 3. In both cases there is a suitable size of pumps for the flow-rates required.

The main differences between the two types are, basically, that membrane pumps are very precise (used for dosing liquids), therefore not needing any flow-rate measuring device, but they require maintenance, that is periodic replacement of the membrane heads, and they are expensive. Gear pumps allow continuous operation with low maintenance. The speed of the gear has a lower limit to avoid its blockage, but this should not be a problem for the flow-rates to be used. In this case the pump will have to operate with a flow measurement device in order to have a reliable online flow measurement. Both pump types can be regulated by means of analogue input signal, changing the rotation speed of the gear pump or the velocity (strokes/minute) of the membrane pump.

In conclusion, from the comparison of the two types of pumps, the gear pumps

seem the preferred option. As a consequence, on line massic measurement devices should be incorporated to the liquid lines. From the different options studied, the equipment proposed for on-line flow-rate measurement is that of Bronkhorst company (see appendix 4). The measurement is based on the thermal conductivity of the liquid. The range of flow-rates that can be measured goes up to 2000 g/h, they are sterilisable and have output electrical signal of 0-5 Vdc or 0(4)-20 mA, that can be used for on-line monitoring of the flow-rates. This is the selected option for flow-rates measurement. A simple alternative of an indirect measurement should be mentioned as well: it consists in the continuous measurement of the weight of the inlet and outlet reservoirs. Variations of their weight with time can be easily translated to flow-rate measurements.

### 3.5 Liquid level

As important as the liquid flow is the maintenance of a known and constant liquid level due to the fact that in continuous culture the growth rate of the bacteria tends to stabilise at a value equal to the dilution rate, which depends both on the flow rate and the culture volume. Common level sensors based on conductivity hypothetically allow to maintain the culture level between pre-defined limits, situated above the level of the output tube (overflow operation). Usually the level sensors fail in its task to determine the limits of the liquid level. The presence of foam, liquid sprinkling due to aeration, and sticking of biomass on the sensors result in the continuous signalling of high volume to the level control system with the result that the output pump always tries to increase its speed in order to decrease the liquid level. This means that the liquid level sensor system is usually inoperative and the volume is actually maintained at the level of the output culture media tube.

As an alternative to common liquid level sensors, based on conductivity measurements, two interesting systems have been identified.

In the first alternative, a long probe (about 1 m, appendix 5) is introduced in the bioreactor. This probe has two pressure sensors. One remains in the head space of the bioreactor. The other one is located at the tip of the probe. The sensor measures the increase in pressure between those two points, which is due to the pressure of the water column. By maintaining this water column constant the liquid level remains

constant. The electronics contained in the probe head supply an output current of 4-20 mA.

In the second alternative (appendix 5), loading cells are located under the bioreactor feet or pedestal. This loading cells transmit the change of the bioreactor weight, allowing to determine the bioreactor liquid volume by determining its weight. The suggested type A can be used up to 300 kg and has a precision of a 0.05% and a repeatability of a 0.01%. Its installation requires to increase the bioreactor height in 81 mm. Final implementation of one of those systems will be decided depending on installation costs and final agreement with the ESA technical officer.

### 3.6. Gas flows.

Gas supply is also an important subject for the bioreactor design. There are mainly two important points to refer to, which are the quantity of gas to supply, and the measurement of the  $O_2$  and  $CO_2$  concentrations of this gas.

The gas supplied to the bioreactor is used to provide the necessary agitation and recirculation of the culture media. For its proper operation a minimal gas superficial velocity of 5 cm/s is needed. That means that in operating conditions it will be necessary to supply an amount of gas between 30 Nl/min and up to 75 Nl/min if possible. This will be attained by using a gas pump able to overcome the pressure created by the water column, while supplying those air flows.

To measure the  $O_2/CO_2$  production and consumption, in the bioreactor it is necessary to maintain the gas pressure and flow to known, and preferably constant, values. The head space of the bioreactor is maintained at a slight overpressure to prevent microbial contamination, by means of a gas pressure measuring/control system. This pressure is also the same in the gas lines going into the gas analysers.

When in the present configuration the gas loop is closed, aspiration of the gas pump results in a decrease of pressure in the head space of the bioreactor. This pressure decrease is due to the fact that part of the air in the head space of the bioreactor is accumulated in the pipe connecting the air pump and the bioreactor. This is necessary in order to increase the pressure under the water column and be able to overcome it. The air removed can be replaced by temporarily opening a gas valve

allowing this way external gas to enter in the part of the loop between the head space of the bioreactor and the pump. Assuming the bioreactor is airtight, once this valve is closed again the pressure before the pump does not decrease again, because no more air is needed to accumulate between the output of the pump and the bioreactor. The only amount of gas that is passing the water column is the one that is being recirculated around the loop. The pressure at the head space and the gas line accessing the gas analysers can be slightly increased and maintained constant by locating a gas flow controller between those gas analysers and the input gas pump. However if the bioreactor has any leak of air, an extra gas input will be needed.

It must be mentioned that if the liquid level is maintained by means of a tube that reaches the liquid surface and a pump that works at a slightly higher flow than the input pump, that is by overflow of liquid, the output pump is also removing, in addition of the culture media, part of the head space gas resulting in a loose of the oxygen enriched gas. The availability of a more efficient liquid level sensor system, would allow to avoid this gas loss. In that case the liquid output tube would be immersed in the liquid and the gas loss in the head space would be avoided.

### 3.8. Control system.

For the proper work of this bioreactor it is necessary to incorporate it in the actual control system network. For this purpose there are available four controllers, of the same type as the ones currently being used (MICON P100). Unfortunately two of them are out of order. As the production of this controllers has been discontinued in favour of more updated models, the only remaining possibilities are either to repair the old ones or to upgrade to new models. The repair of the old ones appears possible, if spare parts can be found, but this option is nearly as expensive as to buy new ones. However buying new ones requires also to upgrade corresponding control the software, because the old version currently being used does not support the new controllers. In any case the upgrade of the system will have to be done in the near future because spare parts will no longer be available and the replacement of the controllers for new ones requires a software update.

For those reasons, conversations have been initiated with a manufacturer (ASTARE) in order to buy 4 new controllers, to be used in this new bioreactor, and

to upgrade the control software. An estimation of the cost of the operation is included in the estimation costs of the equipment. The final decision will be taken after ESA approval.

### 3.9. Other considerations.

As already mentioned, it is proposed to keep the peripheral equipment that have already been used satisfactorily. However, in some cases this peripheral equipment will also be required for the current air-lift bioreactor to work in the compartment II experiments. In addition, the equipment for basic measurement (and control) such as level, pressure, temperature, pH,  $pO_2$ , will also be revised. New equipment purchased when the currently used probes will be required for compartment II. Finally, the equipment for on-line measurement of nitrate concentration already used, will also be used for the new bioreactor.

### 3.10. Economic evaluation.

From preliminary contacts with the suppliers of the equipment, the following economical evaluation of the cost of the set up of the new bioreactor can be done.

ITEM	COST (ptas)	COST (AU)
Reactor	7.000.000	41.200
Lights and light support	1.000.000	5.885
Cooling bath	1.000.000	5,885
DO and pH control system	1.000.000	5.885
CO <sub>2</sub> mass flow meter	250.000	1.471
Gas loop (pump and pressure measurement syst	tem) 750.000	4.414
Liquid pumps	850.000	5.003
Liquid flow meters	250.000	1.471
Power supply	4.000.000	23.542
Controllers and software	3.500.000	20.599
Contingencies	1.000.000	5.885
Total	20.500.000	120.654
taxes (16%)	3.500.000	<u>20.599</u>
Total estimated final cost 20	23.800.000	140.077

### Final remarks.

In this TN a basic definition of the proposal for a new bioreactor for MELISSA compartment IV is presented. Once approved by ESA its set up will be done in two phases. In the first one the final design will be discussed with the manufacturer, in this case Bioengineering. Once accepted for the manufacturer, it is expected a delivery time of around three months. Once the bioreactor will be delivered a second installation phase will be started. During this second phase the control system wiring and tubing connections will be performed. Once completed this second phase the bioreactor will be ready for operation and the experiments currently being done in another airlift will be continued in the new one.

### **References.**

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**APPENDIX 1** 

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### BOENGNEERING Bioengineering AG CH-8636 Wald

Offerte Quote Offre

Prof. F. Godia Unitat D'Enginyera Quimica Facultat de Ciencies Universitat Autonoma de Barcelona E-08193 Bellaterra - Barcelona

8812

Dear Professor Godia

We are pleased to submit you our quotation for

Bioengineering Loop Reactor

CH-8636 Wald, Switzerland December 3rd 1996 / MB

### FERMENTER

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学会の部分で、読みまたのので

### Loop Reactor based on two units of Visual Safety Airlift-Reactor

Sterilizable in situ

basic equipment similar to our description, including

Vessels (each) 26 litres total volume

(total volume of Loop: approx. 53 litres)

cylinder of transparent foil,

inside diameter 150 x 1500 mm,

steel jacket for in situ sterilisation (empty), sampling tube with hypodermic needle

The vessels are connected by stainless steel pipes to a loop, cooling elements are integrated in the connections. On top of the aerated vessel an air separation chamber is mounted with possibility of level control (optional).

Probes can be mounted on top of the vessels and do not reach the illuminated (transparent) part of the vessel.

Lid

stainless steel 1.4435 with sterile and pressure proof ports diameter 19 mm, pressure relief valve and manometer (only for one vessel)

Circulation by air (Airlift)

Aeration (only for one vessel)

pressure control valve, rotameter, check valve, aeration filter (ceramics) in housing (stainless steel), hypodermic needle and aeration tube with ring sparger required air pressure 2 - 7 bar

Ventilation (only for one vessel) exhaust air filter (ceramics) in housing (stainless steel) with pressure holding value

Power Supply 220V / 50Hz

### **Measurements and Controls**

Include an instrument cabinet with tiers 19" high. It accommodates all control loops ordered including

### **Temperature Control**

Sterilizable Pt100 probe, measuring instrument with temperature range 0 -150 C, digital display, temperature controller for heating (during sterilisation) and cooling with two set points for cultivation and sterilization temperature.

Controller parameters are programmable through front keyboard. All necessary in- and outputs, signal 4-20 mA, for data registration and external set point control.

Price for complete loop as described above CHF 68'000.--

### IV CONDITIONS

### **Delivery Time offered**

approx. 4 months following receipt of your written order containing all necessary technical data or on agreement.

### Payment

Within 30 days from date of invoice, strictly net, without any discount, by bank transfer to Union Bank of Switzerland, Uster branch, CH-8610 Uster/Switzerland, Account No. 814.400.01 N

### Terms

Prices are net, ex works, excluding wrapping, without any deduction, excluding V.A.T., according to our General Conditions of Supply, dated 1991, issued by the Swiss Association of Machinery Manufacturers, as per enclosure.

Connection to services and energies such as electricity and mains, installation, commissioning, not included.

### Warranty

1 year, as per Item 13 of the General Conditions of Supply dated 1991, issued by the Swiss Association of Machinery Manufacturers, as per enclosure.

### Installation/Operations Manual

Each Bioengineering fermenter is backed up by

a Manual in English explaining in detail the erection, hook-up to services, start-up, commissioning, maintenance and safety aspects,

a Spare Parts and Accessories Catalogue in English showing in detail with a reference number, a photograph, and a technical explanation all parts available for the unit supplied.

### Validity

This quotation and its prices and terms are valid until March 3. 1997

Yours sincerely Bioengineering AG

2.7. Matthias Bally

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**APPENDIX 2** 

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### **Construction and function**

The new diaphragm dosing pump M 205 Etron M is a reciprocating displacement pump equipped with an efficient electric motor and microcontroller electronics for diverse control applications.

The pump is driven by an overload proof synchronous motor. The rotation of the motor is transformed into the suction and stroke movements of the diaphragm by a precise eccentric tappet - spring system, secondary to the gears.

Thus a defined volume (stroke volume) of the dosing medium is sucked up via the suction valve into the dosing head and displaced through the pressure valve into the dosing line.

The suction and pressure valves are reliable double ball valves.

Mechanical variation of the stroke length at the stroke adjustment knob enables linear adjustment of the dosing output in the ratio 1 : 10.

The integrated microcontroller electronics facilitate the application of the pump to nearly all control tasks occurring in liquid dosing techniques.

The dosing pump can be configured by the customer to the required function via the alphanumeric display with multilingual operator prompting and only four operator buttons (function chart see overleaf).

Mains cable and mains plug are standard equipment of the pump.

### Design variants

The pump variant described in this product information is available in different material combinations of dosing head and valves as well as for different

supply voltages. The pump series M 205 also includes a standard version without electronics and

two electronic versions for simple control applications. For these versions refer to the product

information 1.2/205-01.

# **Dosing equipment**

# Microcontroller -Diaphragm Dosing Pump M 205 Etron M

### Advantages at a glance

- high control function flexibility due to the capable microcontroller electronics
- high dosing precision and linear dosing characteristic
- harmonic dosing process thanks to the electric motor preventing pulsation strokes
- optimal for application in humid locations due to the high degree of protection of the pump
- ideal for the use in laboratories due to the low - noise operation and chemically resistant pump enclosure
- universally resistant, PTFE coated dosing diaphragm
- easy start up by integrated dosing head deaeration with ecologically beneficial medium recirculation into the dosing receptacle



1.2/205-02/11.93E

### Function chart / diaphragm dosing pump M 205 Etron M

- Display operator prompting selectable in German, English or French
- Mains frequency adjustable to 50 or 60 Hz
- Configuration error detection with error indication on the display

### Basic functions

### Manual control

- Continuous operation, stroke frequency selectable 1 121 strokes / min. with 50 Hz and
  1 145 strokes / min. with 60 Hz
  Batch dosing, stroke frequency per batch selectable 1 10.000
- Pulse signal control Proportional dosing, multiplication or devision factor of the input contacts freely selectable Batch dosing, stroke frequency of the batch per input contact selectable 1 - 10.000

	Current signal control
-	Proportional dosing, input signal
	range 0 - 20 mA or 4 - 20 mA and
	20 - 0 mA or 20 - 4 mA selectable

- Measured value dependent control - setpoint of the controlled variable adjustable
- weighting factor for actual value, proportional factor K<sub>p</sub>, reset time T<sub>n</sub>, control direction, control response (linear or logarithmic) selectable

General technical data					
Accuracy	dosing flow ± 1,5 % / linearity ± 4 %				
Suction height*	6 m water gauge (except for 205-0,2)	1			
Materials	parts in contact with media: PP / Viton, dosing diaphragm: PTFE - coated	PVDF / PTFE, steel 1.4571 / Viton			
Drive	synchronous motor optionally 230 V, 1 8,9 W (up to 205-5,0), 23 W (205-6,0 /	10 V. 240 V or 120 V, 50 / 60 Hz, / 205-10 / 205-14)			
Protection	IP 65 (degree of pump protection)				
Weight	ca. 2,8 kg				
Colour	RAL 6017 (May green) / black				
Dosing head - connections	all types except 205-10 and 205-14:         205-10 and 205-14:         DN 4 for           PK / PVC - hose 4/6,         PVC - hose 6/12 or         PP - tube DN 10 (16 x 2),           PVDF - tube 4/6,         PVDF - tube DN 10 (16 x 2),         steel tube 1/4"				
Signal inputs     contact signal input, max. load 5 mA       2 current signal inputs, input load each 22 Ω       input for remote On / Off, contact load 5 mA       input for remote On / Off, contact load 5 mA       input for receptacle empty indication (ALLDOS - empty indication sensor)       Signal outputs       stroke signal output, max. load 250 V / 2 A (ohmic load), contact time 250 msec. / stroke       output empty indication, max. load 250 V / 2 A (ohmic load)					
* Referring to me	dia not viscous and not outgassing				

50 / 60 Hz, with	50 / 60 Hz, with microcontroller electronics E05								
Order number	Stroke cm <sup>3</sup>	l/ h	50 Hz bar	s/ min	l/ h	USg / h	60 Hz bar	psi	s/ min
205-0,2 / E05	0,04	0,3	10	121	0,36	0,095	10	145	145
205-0,8 / E05	0,14	1	10	121	1,20	0,317	10	145	145
205-1,6 / E05	0,22	1,6	10	121	1,92	0,51	10	145	145
205-3,0 / E05	0,42	3	10	121	3,90	1.03	6,8	100	145
205-5,0 / E05	0,69	5	6	121	6	1,58	5	72	145
205-6,0 / E05	0,84	6	8	121	8	2,11	6	90	145
205-10 / E05	1,24	9	6	121	11	2,90	5,5	80	145
205-14 / E05	1,92	14	4	121	17,2	4,54	3	45	145

Version: dosing head and valves of PP, operating voltage 230 V (+'6 % / - 10 %),

Range of further materials for dosing head and valves

Ref. no.*	Material (body / gaskets / valve ball)	
D02	1.4571 / PTFE / 1.4401 without deaeration valve	
D03	PVDF / PTFE / ceramics with deaeration valve	
D57	1.4571 / PTFE / 1.4401 with deaeration valve	

\* When ordering these versions indicate their reference numbers

#### Range of further mains voltages

Ref. no.*	Data
V00	230 V (+ 6 % / - 10 %), 50 / 60 Hz
V01	110 V (+ 10 % / - 10 %), 50 / 60 Hz
V02	240 V (+ 10 % / - 10 %), 50 / 60 Hz
V06	120 V (+ 10 % / - 10 %), 50 / 60 Hz

\* When ordering these versions indicate their reference numbers

Signal transmission cable, 4-core, length 2 m, including circular connector for the panel jack of the pump

Order no.	
321-205	for control signal input and remote On / Off
321-206	for potential-free output for empty indication and stroke signalling.



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R 5/8\*



ALLDOS Eichler GmbH Reetzstr. 85 · D-76327 Pfinztal (Söllingen) Postfach 12 10 · D-76318 Pfinztal Tel. (0 72 40) 61-0, Fax (0 72 40) 61 177 Tx. 7 826 524 dos

Technical data subject to change without notice

182

205-10 and 205-14

# **ProMinent**<sup>®</sup> gamma. Un sistema de dosificación inteligente, programable e interactivo.

Gamma/4 y gamma/5: la nueva generación de bombas dosificadoras electromagnéticas interactivas ProMinent<sup>®</sup> (versión "a"), controladas por microprocesador, que garantiza una gran seguridad en la dosificación en el rango de candales desde 0.01 ml/impulso a 30 l/nora, gracias al control automático del caudal y a la identificación de fallos, incluso de perturbaciones externas.



Dosificación celícuidos y Técnica de recuración exacta 15-JUL-1996 10:50

DE PROMINENT GUGAL

# La facilidad de manejo y la seguridad de funcionamiento garantizan un proceso óptimo.

Las bombas ProMinente gamma son bombas electromagnéticas de membrana, controladas por microprocesador, que se utilizan para la dosificación de líquidos. Estas bombas combinan componentes mecánicos de probada eficacia y la más moderna técnica de control. A partir de la experiencia acumulada durante varias décadas como empresa líder en el mercado de bombas dosificadoras electrónicas, y de las exigencias de los usuarlos, ProMinent\* ha desarrollado una generación completamente nueva de bombas dosificadoras. Las bombas gamma/4 y gamma/ 5. y la bomba dosificadora de precisión mikro g/5, son de fàcil manejo, gracias a indicaciones en texto no cifrado. El diagnóstico de fallos, incluso de perturbaciones externas, garantiza la máxima seguridad de funcionamiento. Las bombas ofrecen posibilidades de adaptación prácticamente ilimitadas para los sistemas de automatización de procesos, garantizando una elevada seguridad de dosificación.

### Componentes mecánicos

### La carcasa

Diseño estético y funcional, de material sintético reforzado con fibra de vidrio, clase de protección IP65. Esto garantiza una gran protección contra productos químicos, así como contra posibles manguerazos. Además, la carcasa de la bomba ProMinent<sup>3</sup> gamma es robusta, resistente a los golpes y de peso reducido.

### El accionamiento magnético

Los sistemas convencionales de accionamiente de una bomba consisten erun motor eléctrico y engranaies, con un gran número de piezas móviles. El accionamiento electromagnético de ProMinent\*. en cambio, cuenta con una única pieza móvil: el inducido del electroimán. En el caso de la bomba ProMinent<sup>2</sup> gamma, se trata de un electroimán de carrera corta con un recorrido máximo de 1.25 mm, que no exige ningún tipo de mantenimiento. La bomba incorpora, asimismo, un modemo sistema de amortiguación de ruidos, que garantiza un funcionamiento silencioso. El ajuste de la longitud de la carrera está acoplado directamente al electroimán. De esto modo, se obtiene una máxima precisión en el ajuste de la carrera, sin retención ni desajuste involuntario.



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### La membrana dosificadora

La membrana dosificadora DEVELOPAN<sup>®</sup> está fabricada en material EPD<sup>M</sup> de alta calidad, reforzado con malla de Nylon, con el núcleo de acero vulcanizado y estás recubierta de Téflon en la parte en contacto con el líquido. La combinación de estos materiales asegura una amplia vida útil a la membrana. La membrana dosificadora DEVELOPAN de ProMinent: es resistente a casi todos los productos químicos y puede utilizarse en un amplio rango de temperaturas, admitiendo contrapresiones de hasta 16 bar.













(SS)

### El cabezal dosificador

Los cabezales dosificadores de las bombas ProMinent" gamma pueden suministrarse en cuatro materiales diferentes:

- polipropileno (PP)
- Plexiglas (NP)
- -Tellón (TT)
- acero inoxidable 1.4571 (SS)

Se han incorporado válvulas de doble bola en la aspiración e impulsión. Los cabezales dosificadores del tipo 1000-0417 PP v NP cuentan, asimismo, con una válvula combinada de purga de aire para facilitar la aspiración cuando la bomba se pone en marcha. Además. la valvuia está provista de un dispositivo de ajuste fino, que controla la desaireación automática en continuo, p. ej. cuando se dosifican líquidos que producen gases. (Los tipos 0423 y 0230 están equipados con válvulas de una bola y no llevan la válvula ce purga de aire.)

Los cabezales dosificadores de la serie HV, fabricados en polipropileno "PP4", han sido diseñados especialmente para líquidos altamente viscosos. Disponen de una mayor sección de paso de líquido, e incorporan válvulas de una bola más grandes, sometidas a la presión de un muelle.

### Amplio rango de voltajes

Las bombas dosificadoras gamma se suministran en dos versiones principales: 230 y 115 voltios, que admiten amplias variaciones de voltaje: de 195 hasta 265 V en el rando superior, y de 98 hasta 132 V en el inferior, para una frecuencia de la rec de 50 o 60 Hz. La versión de 230 V prede suministrarse con enchufe plano, suizo o australiano; la versión de 115 V. con enchufe de EE. UU,

### NUEVO: TÜV-GS

Las bombas dosificadoras gamma tieneu la carantia de comprobacióri. TUV GS y han



sido homologadas según la norma DIN-VDE 0700 y además, contán protegidas contra las interferencias via radio, clase, B, según norma DIN-VDE 0871.



(Seccion transversal del cabeza! en PP)

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# Gracias al control por microprocesador.

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Se puede ampliar el rango de funciones de las bombas dosificadoras de la serie ProMinent<sup>\*</sup> gamma en función de las exigencias especificas del cliente. La versión básica satisface los requenimientos planteados en un gran número de aplicaciones. Si se requieren prestaciones adicionales, se puede incorporar a la versión escogida el correspondiente tipo de control y las funciones opcionales deseadas.

### LA VERSIÓN BÁSICA

### El rango de ajustes

### Operación en continuo

Se pueden regular manualmente el caudal del 100% al 10%, variando la longitud de recorrido mediante un mando giratorio, y, mediante un pulsador, la frecuencia de impulsos "T" desde 120 (100) hasta 1 impulso/minuto, es decir, en el rango 1:1.200 (1:1.000). El número de impulsos: min. seleccionado está indicado. Se incorporan cristales de cuarzo que mantienen con muchísima precisión la frecuencia de los impulsos.

# **IZC** F

### Control externo "Contact"

La frecuencia de impulsos de las bombas dosificadoras ProMinent<sup>®</sup> garma se puede controlar mediante contactos externos, p. ej. por medio de los de un contador de agua. Para ello hay que conectar el cable de control externo a la entrada de contactos de la bomba. Cada impulso recibido (contador de agua o regulador de frecuencia) da un solo impulso a la bomba. La bomba admite un máximo de 120 impulsos/min. No se tiene en cuenta ninguna frecuencia de impuisos que exceda esta cantidad, evitándose. por lo tanto, cualquier sobreexcitación de la bomba.



Contact

### Control de nivel "Minimum"

Se puede conectar en el correspondiente terminal un control de nivel ProMinent<sup>®</sup> de dos etapas para controlar el nivel del líquido. Cuando se alcanza un cierto nivel mínimo, se activa una señal de alarma preventiva. En este caso, se pone en intermitencia la indicación "Minimum" y se enciende el indicador LED rojo y se activa et relé opcional de aviso de fallos, pero la bomba dosificadora sigue funcionando. La bomba se detiene sólo cuando el nivel en el depósito dosificador ha bajado otros 20 mm. Entonces se encienden las indicaciones "Error" y "Minimum". El relé opcional de aviso de fallo continúa cerrado.



### Control de caudal "flow"

La misma bomba dosificadora gamma controla el caudal de dosificación. Se puede instalar en el cabezal dosificador una alarma regulable para controlar el caudal. Una rez conectada, capta cada impulso completo de la bomba. dando una señal de realimentación al circuito electrónico de la misma. Cuando esta señal de realimentación, que indica el caudal correcto, falta durante 8 impulsos seguidos, la bomba se para y se encienden las indicaciones "Error" y "flow" en el display digital, así como el indicador LED rojo.

Error



flow

Manual



La bomba gamma se puede conectar y desconectar, sin potencial, a través del cable de control. Esta función trabaja según el principio de comiente en reposo, es decir, cuando los contactos se abren, la bomba se para y se encienden las indicaciones "Pause" y "Stop".



### Autorregulación

El sistema de mando electrónico de la bomba gamma se autocontrola de manera automática y permanente. En caso de registrar algún fallo de sistema en el microprocesador, la bomba se desconecta y se activa una señal de alarma. Se ponen en intermitencia todas las indicaciones en el display digital y se enciende el indicador LED rojo.

# funciones opcionales. Ud. puede r elegir el tipo de bomba que satisfaga sus exigencias personales.

# CONTROLES **ADICIONALES Y FUN-**CIONES OPCIONALES

### líuminación

Se puede iluminar por detrás el display digital. lo que hace posible una perfecta legibilidad de las indicaciones, incluso en condiciones deficientes de luz o en caso de montaje en un sitio desfavorable. Todos los controles adicionales y las funciones opcionales se pueden suministrar por separado o como paquete combinado libremente.

### Analog Control (control analógico)

Se pueden emplear señales analógicas para controlar de forma proporcional la frecuencia de impulsos entre 0 y 100%. dependiento de la señal (0/4-20 mA). Se puede ajustar el número máximo posible de impulsos por minuto. Si se utiliza una señal analógica de 4-20 mA, la bomba se para y se activa la alarma cuando la señal de entrada es interior a 4 mA (p. ej. en el caso de rotura de cable). Al formular el pedido, se pueden solicitar otras señales de entrada (0-1 V, 0-10 V, 0-60 mV), mediante el código especial de identificación.



# Pulse Control (control de impulsos)

Adapta la bomba ProMinent<sup>o</sup> gamma a cualquier tipo de generadores de impulsos. No es necesario disponer de otras unidades de control. Las siguientes funciones pueden ajustarse mediante pulsadores:

### OTRAS VERSIONES: Tensión reducida 12/24 V y versión RS

Disponemos de las versiones g/4-W y g/4-l de la gamma/4 para tensiones reducidas de 12 V c. c. y 24 V c. a.c. v de la versión g/4-RS con interfase serie RS 232 para control a través de los ordenadores del cliente. Las gamma G/42 para tensiones reducidas, G/4a y G/5a para control por ordenador con interlase RS 232/RS 485 se encuentran en vías de preparación.

### Multiplicación y División de impulsos

La multiplicación y división se define entrando un factor entre 0,01 y 9999, p. ej.: división-entrando con el factor 0,01: (100 impuisos externos = 1 impuiso de

- la bomba)
- 0,25: (4 impulsos externos = 1 impulso de la bomba)
- 1: (1 impulso externo = 7 impulso de (admod Sl
- Multiplicación entrando el factor 4: (1 impulso externo = 4 impulsos de la bomba)
- 9999: (1 impulso externo = 9999 impulsos de la bomba)

Contador de preselección "N --El número de impulsos preseleccionado. p. ej. 20 (máx. 9999) se activa mediante un contacto libre de potencial o el pulsador P. indicándose el número de impulsos pen-

#### dientes en el display digital. Memoria "Mem."

Se puede conectar adicionalmente una memoria intermedia, con una capacidad de almacenamiento de 65.535 (215-1) impulsos. Si la frecuencia de los impulsos recibidos es supenor a la frecuencia máxima de la bomba. éstos quedan almacenados y la bomba continua dosificando hasta finalizar la secuencia. Es decir. se puede emplear una bomba dosificadora de menor capacidad en algunas aplicaciones. Esto es un ejemplo concreto de como se pueden minimizar los costos.



### Contador de impulsos "N"

Totalizador del número de impuísos, hasta un máximo de 19998 impulsos.

### **FUNCIONES OPCIONALES**

### Temporizador

Esta función permite programar hasta 31 tiempos de dosificación, con reiteración diaria o semanal y con intervalos de 1 minuto a 24 horas. Se utiliza p. ej. para la dosificación automática de microbicidas. para tratamientos de choque en la industria. del papel y en torres de refrigeración contra la formación de algas y limos.

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Manual

### Salida de relé

Sirve para la teletransmisión de señales, p. ej. del aviso de fallo a la central de mando, o bien para el control externo de p. ej. una segunda bomba dosificadora ProMinent<sup>®</sup> que trabaja en régimen sincronizado. Posibilidades de ajuste:

### Alarma general

Alarma previa del control de nivel y desconexión final de la bomba, control de dosificación, fallos del sistema, aviso de fallo de los fusibles y de la red. Principo de funcionamiento: el relé vuelve al estado de resposo en caso de alarma (normalmente cerrado).

### Relé de alarma

Alarma previa del control de nivel y desconexión final de la bomba, control de dosificación, fallos del sistema. El relé se excita en caso de alarma (normalmente abierto).

### Relé generador de impulsos

Con generación de impulsos paralelos a cada impulso del electroimán de la bomba; duración del contacto: 150 mseg. La función deseada debe especificarse en el pedido.

### ProMinent Remote Control

La combinación ProMinent® Remote Control, compuesta por una bomba dosificadora gamma G/4Ra o G/5Ra y un mardo a distancia, permite controlar y operar la bomba desde una distancia de haste 100 m.

### ProMinent mikro g/5

Es una bomba dosificadora interactiva de precisión, controlada por microprocesador, de uso en laboratorios y la industria. La carcasa. el manejo y las opciones de la mikro MG5a son idénticos a los de la gamma G/5a. Tiene un rango de caudales desde 1 ul/impulso a 1500 ml/hora: la presión de trabajo máx. es de 40 bar y la precisión de dosificación es superior a  $\pm$  0.5%. Les facilitaremos gustosamente información más detallada, si Vds. la solicitar.



Se precisa una comba dosificadora con una capacidad máx. de 1,8 i/h para cosificar, en función del caudal, silicato sódico concentrado en una tuberra de agua potabel, a una contramesión de 6 bar. La bomba se controlará a través de los contactos de un contador de agua ya existente, con un intervalo de impulsos excessivo, o bien a través de un caudalimetro magnético-inductivo (IDM), con una señal de 4-20 mA. En caso de fallos, se debe activar la correspondiente alarma en la central, y la bomba debe tener un sistema de seguridad para evitar que sea manipulada por personas no autorizadas. Será instalada en Francia.



N. 6 6. 1

DE PROMINENT GUGAL

15-JUL-1996 10:54 DIMENSIONES

gamma/4, gamma/5

gamma/4		A	В				·
1000, 1601	PP	232	196			EF	G
1201	NP	230	170	17	70	6x4 81	- 38
	11	213	173	19	/0	6x4 81	38
	SSI	211	164	25	60	6x4 79	38
	SK1	211	162	34	60	<b>6x5</b> 79	- 38
0703	PP	222	102		. 60	<u>1x8</u> 79	38
	NP	230	100	17	70	6x4 81	38
	Π	212	179	-19	70	6x4 8	38
	SS1	213	178	20	70	6x4 7.9	. 38
1002 0308	DD	611	103	29	70	6x5 79	.38
1002.0008		225	186	17	70	8x5 76	50
		223	187	11 - T	85	8x5 76	50
•	551	216	206	8	80	8x5 79	50
0015		214	206	-8	80	8x7 77	50
UZ IS	PP	225	197	6	90	1219 76	
	NP	223	195	. 3	100	12-0 70	66
	11	216	214	-16	95	1249. 70	66
	551	214	209 .	-11	95	12-10 75	66
1002 HV	PP4	214	172	-4	70	DN 10 77	
gamma/5						Divito Bu	50
1602 a 1006	PP	271	. 207	20	70		
	NP	269	208	32	70	8x5 95	50
	TT	259	208	13	00	<b>5</b> 55 55	50
	SSI	259	220	20	. eo	8x5 97	50
(a): 1310 a	PP	271	218			827 97	50
0613	NP	269	216	2/	90	8x5/12x9 95	66
(b): 0813 a	π	259	210	24	100	8x5/12x9 95	66
0417	\$S1	259	230	44	95	8x5/12x9 97	66
0423 a 0230	PP	260	2.50		95	8x7/12x10 97	66
	NP	200	2/5	-18	135	DN 10-23x16 95	117
	<b>T</b>	250	2/5	-18	135	DN 10-23x16 96	117
	SS1	230	234	· <u>7</u>	135	DN 10-d16 95	117
IOOS HN	004	400	234	7	135	DN 10-3/8" 95	117
	P74	269	193	47	85	DN 15 103	
1812 HV	PP4	270	193	47	85	DN 15 104	50 5
		269	200	40	100	DN 15 104	. 00

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163 1000-0417 PP y NP





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PAG.07 10:56

# 15-JUL-1996 10:55 DE PROMINENT GUGAL! gamma/4, gamma/5

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PAG.08 10:57

omb Jamn	le la la	Cauda contra máxim	nia presión Na		Cauc contr	lal a apresión		Frecuencia de impulsos	Conexión* Ø ext. x	Altura de aspiración	Peso	:
		bar	٧'n	mVimpulsos	bar	ື Vh	ml/impulsos	min	12 int.	mCA ·	ko	
am	na/4		_		_						Ng	
<b>3/4a</b>	1000	10	0.20	0.028	5	0.26	0.026	100				· · .
	1601	16	0.90	0 125	2	0,20	0.035	120	6x4	1,5	2,7- 3	4
	1201	12	1 55	0.215	0	1,17	0.16	120	6x4	6	27- 3	4
	0703	7	3 40	0,215	0	1,80	0,25	120	6x4	. 6	2.7- 3	4
	1002	10	2,00	0.00	3.3	3,67	0.51	120	6x4	3	2.7- 3	4
	0308		2,03	0,29	5	2,81	0,39	120	8×5	6	29-4	
	0215	1 5	140	1,08	1.5	8,5	1,18	120	8x5	6	29 4	
		1.5	14.0	2.05	1	15.8	2,20	120	12x9	1.5	31. 4	' <del>7</del>
- MUU	na/5										• • •	
/5a	1602	16	2.09	0.29	8	274	0.38	120				:
	1605	16	4,74	0.79	ě.	5 76	0.00	120	SXS	6 · ·	4.6 5,	,8 ∵
•	1006	10	5.83	0.81	ž	7.06	0.50	100	8X5	6.	6,7- 7.	9
	1310	13	9.54	1 50	-6	7.00	0,98	120	8x5	<b>.</b>	4,6- 5.	8
	0613	6	13 1	1.82	2	10,6	1,0	100	8x5	6	6.9- 8	5 -
	0813	· g	13.2	3.04	3	14.9	2.08	120	8x5	5,5	4.8- 6	4
	0417	2 E	17.2	5.CI	4	14,6	2.44	100	12 x 9	6	69. 8	5
	0/22	0.0 5 F	17,4	2,42	2	17.9	2.48	120	12 x 9	4.5	4 8. 5	A
•	0720	3,3	22,5	3,75	2	24.6	4,10	100	DN 10	5		
	U23U	2	30,3	4,21	1	34,5	4,80	120	DN 10	25		<b>*</b>
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		v	19,9	2.21	4	14,6	2.44	100	DN 15		A	•
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### **APPENDIX 3**

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# MICROPUMP® PUMP TECHNOLOGY

The following Introduction explains the basic technology behind magnetically coupled gear pumps and helps you to differentlate between the two types of MICROPUMP\* pump heads offered—conventional cavity-style and pressure-loaded.

Large arrows indicate discharge pressure; smaller arrows show direction of gear rotation and fluid flow.

Magnetically coupled gear pumps are designed for pulseless fluid delivery at low to moderate flow rate and pressure. They operate via two or three rotating gears. One of the gears is turned by a power source (via magnetic coupling) and drives the other gear(s). The spaces between the gear teeth carry the fluid from the inlet to the outlet as shown above.

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Gear pumps can pass air bubbles and still maintain their prime. Some gear pumps can attain maximum pressure with practically no loss in flow.



Magnetically coupled gear pumps eliminate shaft seals-ensure freedom from leaks and contamination. The conventional means of sealing pumps is by using some type of

dynamic seal (i.e., a seal created on a moving shaft) which allows possible areas for leakage, creates additional friction for the motor to overcome, and often generates heat

# HOW TO CHOOSE YOUR PUMP HEAD AND MOTOR

We offer this high-quality line of pump heads and motors as separate components to let you create a pumping system that meets your specific requirements. To help determine the best combination of pump head and motor for you needs. consider the following factors.

FLUID CHARACTERISTICS Consider the chemical compatibility, viscosity, and temperature of the fluid. Determine also whether the fluid is shear sensitive, is sensitive to particles shed from gear wear, or contains particles. Gear pumps are not well suited for shearsensitive fluids or fluids which are sensitive to particles from gear wear. Gear pumps are particularly well suited for viscous fluids up to 1500 centipoise.

SYSTEM CHARACTERISTICS ---- Consider your desired flow rate, differential pressure, and system pressure. MICROPUMP\* pump heads handle flow rates up to 68 LPM (18 GPM), differential pressures up to 100 psi, and system pressures up to 1500 psi.

Determine whether the inlet will be flooded, pressurized, or requiring a suction lift. If the inlet is flooded, use either a conventional cavity-style or a pressure-loaded pump head. If the inlet is pressurized or a suction lift is needed, use a cavity-style pump head. If the initial differential pressure will be high, use a pressure-loaded pump head.

Choose a pump head without a canister, with standard or large canisters, or with NEMA Type 56 C-face flange adapters according to your required motor mounting configuration.

MAINTENANCE REQUIREMENTS-Depending on your application, your pump maintenance may simply include such routine procedures as the occasional replacement of gears and

bearings on pump heads or the replacement of brushes on brushed motors. Or you may need to sterilize the pump head between runs or between successive applications.

Cavity-style pump heads with Teflon®, Ryton® or graphite gears can be autoclaved intact or after disassembly (do not exceed 250°F temperatures for the Teflon and Ryton gears). Use only chemicals to sterilize pressureloaded pump heads with Ryton gears.

DRIVE REQUIREMENTS --- Consider the motor and control requirements of your application. The MICROPUMP system lets you use an AC, DC, or pneumatically driven motor; a continuous- or intermittent-duty motor; or a fixed- or variable-speed motor with manual or external controls. Cole-Parmer offers a wide selection of drives from simple fixed-speed AC motors to variable-speed drives with digital display, timer, and remote control or computer interface capability. We also have adapters for NEMA Type 56 C-face motors and IEC/ISO 63 or 71 frame metric motors.



## CAVITY-STYLE PUMP HEADS

Series A, B, E, and F pump heads use conventional cavity-style gear technology. These cavity-style pump heads feature suction lift capabilities, are easier to clean and service, and are less expensive than the pressureloaded type.

Cavity-style gear pumps do not use a suction shoe but depend on the surrounding pressure in the magnet cup cavity to hold the gears tightly together. Since it is imperative that the gear tips mesh exactly, cavity-style pump heads often use helical gears composed of extremely low friction material-such as Teflon®.

# Positive displacement: Gear



## PRESSURE-LOADED PUMP HEADS

Series C. D. G. and H pump heads are pressure loaded, thus increasing the volumetric efficiency of the pump. Pressure-loaded pump heads use a suction shoe which works with the fluid pressure in the magnet cup to seal the gears tightly together.

The higher the discharge pressure on the suction shoe and mesh point, the higher the efficiency of the pump. While operating, the magnetic cup is filled with the fluid being pumped. The suction PRESSURE DISCH shoe is positioned around the inlet and meshing point (see diagram at right). The pressure on the outlet side of the pump should be greater than the pressure on the inlet side to force the suction shoe and gears together. In this manner, the suction shoe ensures that fluid transport is complete-with no backflow or leakage between gear tips.



PUMPS

# MICROPUMP® PUMP HEAD AND MOTOR COMPATIBILITY GUIDE

Use the following charts to compare the maximum flow rates that are achievable with various motor and MICROPUMP® pump head combinations. Maximum flow rates (given in ml/min) were determined under conditions of nominal back pressure.

For a complete description of each motor, see the "Motors" section on pages 741-745. For details on pump heads, see pages 1130-1132.

# MOTORS FOR MICROPUMP® PUMP HEADS WITHOUT CANISTER (SERIES A AND C)

Mator	Max motor	Maximum flow rate (r	Maximum flow rate (ml/min) using indicated pump head model at given speed									
model	speed	Series A cavity-style		Series C pre	pressure-loaded							
number	(rpm)	07002-20	07002-32	07002-33	07002-35	07002-12						
07002 20	500	N/R	8.5	20	40	N/R						
07002-39	000	1020	N/B	N/R	N/R	N/R						
07002-42	6000	1920	107	005	670	740						
07002-38	8000	N/R	135	335	070							

\*N/R = not recommended for use with indicated motor.

### MOTORS FOR MICROPUMP® PUMP HEADS WITH STANDARD CANISTER (SERIES B AND D)

							table at a sta	diasted put	no bead m	odel et dive	n speed*		
Motor	Max motor			Ma	ximum flow	rate (ml/m	iin) using in	dicated put	np neau m	arias D nre	ssure-loade	ed	
model	speed		S	eries B cav	ity-style	·			07000.00	07000 07	07002-14	07003-02	07003-04
number	(rpm)	07002-16	07002-17	07002-23	07001-80	07001-70	07001-40	07002-25	07002-26	0/002-2/	0/002-14	0700-02	1600
07002-58	1550	495	495	990	990	1040	1460	25	65	130	145	8/0	2200
07002-30	2000	060	960	1920	1920	2000	2800	50	125	250	275	1690	3300
0/144-93, -94	3000	1010	1010	2000	2000	2100	3000	55	130	265	290	1780	3400
07144-95, 07003-83	3150	1010	1010	2000	2000							1	
07144-00, -02, 07144-05, -07, 75210-00, -05,	3600	1150	1150	2300	2300	2400	3400	60	150	300	330	2000	3900
75210-10, -15						<u> </u>			170	225	370	2300	4400
07003-90, 78200-22,	4000	1280	1280	2600	2600	2700	3800	70	170	335			
10200-21, 07144-31			1000	0000	2000	3300	4700	85	210	420	460	N/R	N/R
07617-75 -77	5000	1600	1600	3200	3200			ļ			<u> </u>		+
07617-70, -72	6100	1950	1950	3900	3900	4100	5700	105	255	510	560	3400	6600
78004-00	0100					5400	7500	135	335	670	735	4500	8700
07144-97	8000	2600	2600	5100	5100	5400	- 1300	- 135	+			1	0000
07002-44, -45, 07002-46, -47	9000	2900	2900	5800	5800	N/R	N/R	N/R	N/R	760	830	N/R	9800

N/R = not recommended for use with indicated motor.

### MOTORS FOR MICROPUMP\* PUMP HEADS WITH LARGE CANISTER (SERIES E AND G)

	Мах	Maximum flow rate (ml/min) using indicated pump head model at given speed*									
model motor number (rpm)		Series E cavity-style	Series G pressure-loaded								
		07001-52	07003-06	07003-08	07003-30	07003-31					
07003-36	3150	9000	N/R	5000	N/R	N/R					
07003-37	3200	9200	2700	5100	5500	11,100					
07002-43	3400	9700	2900	N/R	N/R	11,800					
07002-51	4300	N/R	N/R N/R 7400 N/R								

\*N/R = not recommended for use with indicated motor.

### NEMA TYPE 56 C-FACE MOTORS FOR MICROPUMP\* PUMP HEADS WITH NEMA TYPE 56 C-FACE FLANGE ADAPTER (SERIES F AND H)

Max	N mo	faximum fle del with an	ow rate (m iy NEMA T	l/min) using ype 56C-fa	g indicated	pump hea t given sp	eed			
speed	Serie	s F cavity-	style	Series H pressure-loaded						
(rpm)	07001-54	07003-25	07003-27	07003-34	07003-35	07003-32	07003-33			
1725 3450	4900 9900	10,400 20,700	33,300 66,600	1500 2900	2800 5500	3000 6000	6000 11,900			

MICROPUMP—Reg TM Micropump Corp. Ryton-Reg TM Phillips Petroleum Co.

Teflon-Reg TM E. I. du Pont de Nemours & Co.



Easily interchangeable on various motors

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Pulse-free flow

These MICROPUMP® pump heads feature an enclosed gear assembly designed for smooth, quiet operation. Driven magnets are encapsulated in 316 stainless steel (SS) and either Teflon® PTFE or Ryton® for good durability and chemical resistance. All-plastic PVDF and Teflon® PTFE pump heads are available—call for details.

Use series A through D (on pages 1130-1131) for your low-flow general-purpose applications—up to 7500 ml/min. Models with an internal bypass valve recirculate excess discharge pressure to the inlet side of the pump to protect the pump head and entire system from excessive pressures. Use series E through H (on page 1132) for your highcapacity applications—up to 38.6 liters/min.

Use the flow performance graphs on pages 1130-1132 for guidance in choosing the best pump head for your application. The graphs and

■ Teflon<sup>®</sup> PTFE, Ryton<sup>®</sup>, or graphite gears

tables are color-coded according to materials of construction; refer to the pump head ordering tables for the specific materials. See page 1129 for the maximum flow rates of specific pump head and motor combinations.

MICROPUMP pump heads feature a 1/8" NPT(F) port size and are interchangeable to satisfy a variety of flow rate, pressure, and fluid compatibility requirements. All of these pump heads can be used with the motors identified on page 1129.

Optional service kits contain gears, bushings, seals, and suction shoe (for pressure-loaded pump heads); order kits separately from pump head ordering tables.

MICROPUMP—Reg TM Micropump Corp. Ryton—Reg TM Phillips Petroleum Co. Teflon, Viton—Reg TM E. I. du Pont de Nemours & Co.

#### CAVITY-STYLE PUMP HEADS These conventional cavity-style pump heads provide nominal flow rates Pump head 07002-23 with from 1100 to 3200 ml/min (see table below). Ports are 1/8" NPT(F). internal bypass valve Choose series A pump head (model 07002-20) for motors that do not require a canister for mounting. Select any series B pump head for motors that require a standard canister for mounting. Series B pump heads are available with an internal bypass valve. Pump head 07002-20 without canister Pump head 07001-70 with standard canister 80 80 07001-40 07001-70 07002-20. 07001-23 70 70 07002-16. 105 07001-80 07002-17 41 E $D = \lambda^{-1} \lambda^{-1}$ 60 60 60 90 10 -2 5.18 3450 rpm ressure (psi) 75 50 (psi) (psi 50 (asi 3450 $i \neq \gamma$ 3450 rpm Pressure Pressure Pressure 40 40 40 60 1750 1750 rpm 30 45 1 1750 rpm 20 20 30 $\mathbf{N}$ 10 15 10 875 rpm 875 rpm 875 rpm 19 20 O 0 0 2250 3000 3 1800 2400 Ó 750 1500 1200 1800 600 1200 n 300 600 900 0 600 1200 2400 0 Flow (ml/min) Flow (ml/min) Flow (ml/min) Flow (ml/min) Service kits Materials of construction Nominal Max Max Temperature Bypass Max Catalog Catalog Price system Series mi/rev flow rate diff Price Body Gears Seals rpm range valve number numbe (ml/min) osi psi Cavity-style pump heads without canister -50 to 130°F1 H-07002-10 \$136.00 9000 No \$405.00 316 SS Teflon PTFE Teflon PTFE H-07002-20 0.32 1100 300 45 Α Cavity-style pump heads with standard canister H-07144-38 H-07144-38 Teflon PTFE Teflon PTFE 9000 -50 to 130°F No 405.00 136.00 316 SS H-07002-16 0.32 1100 300 45 B 316 SS Tefion PTFE Teflon PTFE 9000 -50 to 130°F1 Yes 405.00 136.00 H-07002-17 0.32 300 45 в 1100 H-07002-08 -50 to 130°F1 84.50 H-07002-23 300 **\***45 316 SS Teflon PTFE Teflon PTFE 9000 Yes 373.00 0.64 2200 в Teflon PTFE -50 to 250°F Yes H-07001-89 84.50 45 316 SS Ryton 9000 373.00 H-07001-80 0.64 2200 300 в Viton Ryton Ryton/ 9000 -50 to 150°F Yes 267.00 200 45 в H-07001-70 0.67 2310 316 SS Yes H-07001-41 316 SS Teflon PTFE Teflon PTFE 8000 -50 to 210°F 373.00 84.50 45 H-07001-40 0.94 3240 300 в Nominal flow rate pumping water with no back pressure at 3450 rpm. 'Up to 210°F using the high-temperature seals below. H-07002-05 High-temperature Teflon FEP seals let you use pump heads 07002-16, -17, -20, and -23 (this page) and 07002-12, -25, -26, and -27 (facing page) at temperatures up to 210°F. Pack of two seals......\$5.90/p



<u> </u>			Al astant	Mari	May	Ma	terials of con	struction		<b>-</b> .		1	Service	<u>kits</u>
Series	Catalog number	ml/rev	flow rate (ml/min)*	system psi	diff psi	Body	Gears	Seals	Max rpm	lemperature range	valve	Price	Catalog number	Price
Pressure-loaded pump heads without canister														
C	H-07002-32 H-07002-33	0.017	55 140 290	300 300 300	50 50 60	316 SS 316 SS 316 SS	Graphite Graphite Graphite	Teflon PTFE Teflon PTFE Teflon PTFE	8000 8000 8000	-50 to 250°F -50 to 250°F -50 to 250°F	No No No	\$419.00 419.00 419.00	H-07144-42 H-07144-44 H-07144-47	\$141.00 141.00 141.00
	H-07002-35	0.004	310	300	50	316 SS	Ryton	Teflon PTFE	9000	-50 to 130°F1	No	419.00	H-07144-36	141.00
		n hoads	with ctan	dard ca	nister									
D D D	H-07002-25 H-07002-26	0.017	55 140	300 300	50 50	316 SS 316 SS 316 SS	Graphite Graphite Graphite	Teflon PTFE Teflon PTFE Teflon PTFE	9000 9000 9000	-50 to 250°F -50 to 250°F -50 to 250°F	No Yes Yes	419.00 419.00 419.00	H-07144-42 H-07144-44 H-07144-47	141.00 141.00 141.00
	H-07002-27	0.084	290	300	50	316 SS	Byton	Teflon PTFE	9000	-50 to 210°F	Yes	419.00	H-07144-34	141.00
D	H-07002-14 H-07003-02 H-07003-04	0.564	1940 3760	300 300	50 50 45	316 SS 316 SS	Ryton Ryton	Viton Viton	8000 9000	-50 to 210°F -50 to 250°F	Yes Yes	392.00 392.00	H-07003-12 H-07003-14	101.00 101.00
'Nominal	Vorninal flow rate pumping water with no back pressure at 3450 rpm. Up to 210°F using the high-temperature seals on facing page.													

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Cavity	-style pump he	ads wit	h NEMA Ty	pe 56 C	-face f	lange ad	apter							
ㅋ ㅋ ㅋ	H-07001-54 H-07003-25 H-07003-27	2.86 6.00 19.30	9.8 20.8 38.6	300 500 500	45 70 100	316 SS 316 SS 316 SS	Teflon PTFE Teflon PTFE Teflon PTFE	Teflon PTFE Teflon PTFE Teflon PTFE	3450 4000 4000	32 to 125°F -50 to 210°F -50 to 210°F	No No No	1710.00 2400.00 4450.00	H-07001-55 H-07003-26	357.00 627.00
Press	ure-loaded pum	np head	s with large	e caniste	er			•••••		· · · · · · · · · · · · · · · · · · ·		1		L
G G G G	H-07003-06 H-07003-08 H-07003-30 H-07003-31	0.85 1.60 1.73 3.46	3.0 5.2 6.0 12.3	1500 1500 1000 1000	60 60 50 50	316 SS 316 SS 316 SS 316 SS 316 SS	Ryton <sup>●</sup> Ryton Ryton Ryton	Viton <sup>®</sup> Viton Viton Viton	8000 6000 6000 4000	50 to 250°F 50 to 250°F 50 to 250°F 50 to 250°F	No No No No	816.00 816.00 855.00 855.00	H-07003-16 H-07003-18 H-07003-38 H-07003-39	114.00 114.00 114.00 114.00
Press	ure-loaded pum	p heads	s with NEM	A Type	56 C-fa	ace flang	e adapter							
ннн	H-07003-34 H-07003-35 H-07003-32 H-07003-33	0.85 1.60 1.73 3.46	3.0 5.2 6.0 12.3	1500 1500 1000 1000	60 60 50 50	316 SS 316 SS 316 SS 316 SS 316 SS	Ryton Ryton Ryton Ryton Ryton	Viton Viton Viton Viton	8000 6000 6000 4000	50 to 250°F 50 to 250°F 50 to 250°F 50 to 250°F	No No No No	1050.00 1050.00 1080.00 1080.00	H-07003-17 H-07003-19 H-07003-38 H-07003-39	114.00 114.00 114.00 114.00
*Nominal	flow at 3450 rpm p	oumping v	vater with no	back pres	sure.				·			4		

MICROPUMP-Reg TM Micropump Corp.

Ryton-Reg TM Phillips Petroleum Co.

Teflon, Viton-Reg TM E. I. du Pont de Nemours & Co.

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Use the flow capacity values (see page 1129 for series A and C; see second table below for series B and D) to determine the best combination of motor and MICROPUMP pump head for your pumping needs.

### MOTOR SPECIFICATIONS AND ORDERING INFORMATION

Catalog	Туре	rpm	Frame	Motor	hp	Power source	Termination	Dimensions L x W x H	Shpg wt Ibs (kg)	Price			
number	the base of the rate of OPPIMP nume baseds without consister (series A and C). See page 1129 for maximum flow capacities.												
H-07002-39 H-07002-42 H-07002-38	DC DC DC DC	500 6000 8000	TENV TENV TENV	PM brush PM brush PM brush	0.005 0.015 0.01	0 to 24 VDC, 0.60 A 0 to 12 VDC, 2.50 A 0 to 24 VDC, 0.50 A	Alligator clip Alligator clip Alligator clip	4" x 1½" x 1¾" 3¼" x 1½" x 1½" 3¼" x 1½" x 1½"	1 (0.5) 1 (0.5) 1 (0.5)	\$235.00 172.00 197.00			
Hutor, for re	In the factor of the standard canister (series B and D). See flow capacities table below.												
H-07144-91	DC DC	4000	TENV TENV	PM brush PM brush	0.12 0.12	0 to 12 VDC, 4 A 0 to 24 VDC, 3 A	13" wire leads 13" wire leads	4" x 3" x 3" 4" x 3" x 3"	3 (1.4) 3 (1.4)	158.00 158.00			
H-07002-58 H-07144-93	AC AC	1550 3000	TEFC TEFC	Shaded pole Shaded pole	0.05 0.05 0.1	115/230 VAC, 50/60 Hz, 1.5 A 115 VAC, 50/60 Hz, 1.9 A 115/230 VAC, 50/60 Hz, 1.4 A	12" wire leads 6-ft cord & plug 19" wire leads	5¼" x 4 x 4¼" 5¼" x 4 x 4¼" 6" x 5¼" x 5"	6 (2.7) 7 (3.2) 7 (3.2)	223.00 223.00 294.00			
H-07144-94 H-07002-44 H-07002-45 H-07002-46	AC/DC* AC/DC, v-spd* AC/DC v-spd*	9000 9000 9000 9000	Open Open Open Open	Brush Brush Brush Brush Brush	0.123 0.123 0.123 0.123 0.123	115 VAC, 50/60 Hz, 2.1 A 115 VAC, 50/60 Hz, 2.1 A 230 VAC, 50/60 Hz, 1.1 A 230 VAC, 50/60 Hz, 1.1 A	6-ft cord & plug 8-ft cord & plug 6-ft cord 6-ft cord	5½" x 3¼" x 4" 5½" x 5 x 3¼" 5½" x 3¼" x 4" 5½" x 3¼" x 4" 5½" x 5" x 3¼"	5 (2.3) 6 (2.7) 5 (2.3) 6 (2.7)	261.00 361.00 361.00 361.00			
H-07144-95 H-07144-97	XPRF <sup>1</sup> Air driven	3150 8000	NEMA 42 TENV	PSC Vane	0.17 0.13 to 0.29	115/230 VAC, 50/60 Hz, 1.8 A 5 to 11 SCFM; 5 to 80 psi	6" wire leads 1/8" NPT(F)	11" x 6" x 5¼" 3¾" x 3" x 5¼"	20 (9.1) 3 (1.4)	634.00 311.00			

07144-95

**Order MICROPUMP®** 

pump heads separately.

For intermittent use only. Rated for NEMA Class I, Groups C and D, Division 1 hazardous environments.

### FLOW CAPACITIES FOR MICROPUMP® PUMP HEADS WITH STANDARD CANISTER

				Flov	v rates (liters/min)	using indicated pump mo	otors	
	Pump heads		07000 50	07144-02-04	07144-95	07003-90.07144-91	07144-97**	07002-44, -45, -46, -47
Series	Model number(s)	ml/rev	1550 rpm	3000 rpm	3150 rpm	4000 rpm	8000 rpm	9000 rpm
D D D	07002-25 07002-26 07002-27 07002-14	0.017 0.042 0.084 0.092	0.026 0.065 0.130 0.143	0.051 0.126 0.252 0.276	0.054 0.132 0.265 0.290	0.068 0.168 0.336 0.368	0.136 0.336 0.672 0.736	0.828
B	07002-14	0.316	0.490	0.948	0.995	1.26	2.53	2.84
<u> </u>	07003-02	0.564	0.874	1.69*	1.78	2.26	4.51	5.08'
B B B B	07002-23 07001-80 07001-70 07001-40	0.640 0.640 0.670 0.94	0.992 0.992 1.04 1.46	1.92 1.92 2.01 2.82	2.02 2.02 2.11 2.96	2.56 2.56 2.68 3.76	5.12 5.12 5.36 7.52	5.76 <sup>1</sup> 5.76 <sup>1</sup> 6.03
	07003-04	1.090	1.69	3.27'	3.43	4.36	8.72	<u> </u>

B 07005-04 1.0000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000

# POWER SUPPLIES/SPEED CONTROLLERS

Provide DC output for small motors, metering pumps, and more

These compact controllers rectify 115 VAC to either 12 VDC (models 02630-25 and -90) or 20 VDC (models 02630-85, -95, and -87). Manual models provide a constant, preselected VDC output. Automatic models respond to standard analog inputs (1-5 mA, 4-20 mA, 0-5 V) from control instruments. Output voltage adjusts continuously, proportional to input signal.

Automatic models feature offset and span adjustments and IR compensation. Offset and span adjustments let you adjust VDC output to any input range. IR compensation increases amperage output to maintain constant speeds under increasing loads.

Units measure just 734"L x 512"W x 4316"H. All models come with a 6-ft, three-wire, UL-listed cord with plug and a 2-amp fuse. Because the primary side of the transformer is fused, both primary and secondary circuits are protected.





Manual controller

Automatic controller

Catalog number	Туре	Output	Shpg wt Ibs (kg)	Price
H-02630-25	Manual	1 to 12 VDC, 7 amps	6 (2.7)	\$235.00
H-02630-90	Automatic	1 to 12 VDC, 7 amps	6 (2.7)	359.00
H-02630-85	Manual	2 to 20 VDC, 3.5 amps	7 (3.2)	235.00
H-02630-95	Automatic	2 to 20 VDC, 3.5 amps	6 (2.7)	359.00
H-02630-87	Manual	2 to 20 VDC, 7 amps	9 (4.1)	294.00

## COLE-PARMER® VARIABLE-SPEED DRIVES

Use these continuous-duty drives with MICROPUMP® pump heads with standard canister (series B and D sold on facing page); get flow rates up to 3900 ml/min. Drives feature a  $\frac{1}{10}$  hp DC motor with high-torque magnetic coupler and mounting adapter. Speed control is adjustable from 180 to 3600 rpm via single-turn potentiometer. Maximum differential pressure is 50 psi. Soft-start feature allows gradual one-second acceleration to any chosen speed for smooth, pulseless flow rate changes.

### MOTOR/CONTROLLER SYSTEM



System comes complete with controller connected to a motor via a 6-ft cable. Controller features exceptional line/load regulation of ±2% b-tt cable. Controller reatures exceptional line/load regulation of  $\pm 270$ and improved regulation of motor current, which minimizes magnetic drive decoupling. Solid-state controller is UL-listed under UL508, is CSA-certified, and has an IP53 rating. Controller measures 7"W x 31/4"H x 51/4"D.

Motor includes a welded base for mounted or for free-standing use. Motor has an IP21 rating; comes with a 6-ft power cord with U.S. standard plug on 115 VAC model (European plug on 230 VAC model; other plug types available on request). Motor measures 613/16"L x 413/16"W x 35/8"H.

H-07144-05 Continuous-duty motor/controller_system	
115 VAC, 50/60 Hz. Shpg wt 9 lbs (4.1 kg)	\$600.00
H-07144-07 Continuous-duty motor/controller system; 220 VAC, 50/60 Hz. Shpg wt 9 lbs (4.1 kg)	\$600.00
H-07144-08 Replacement controller for model 07144-05. Shpg wt 3 lbs (1.4 kg)	\$241.00
H-07144-09 Replacement controller for model 07144-07. Shpg wt 3 lbs (1.4 kg)	\$241.00

### CONSOLE DRIVE

Motor and controller are enclosed in a case that has carrying handle and feet. Adjust speed using the frontpanel potentiometer or by remote control-a 1/4" phone jack port accepts a 4-20 mA input signal. Remote control linearity is better than ±3% FS. Both models include 6-ft power cord; 115 VAC model includes plug. Units have an IP22 rating and measure 117/16"L x 67/16"W



x 51/16"H. Shpg wt 10 lbs (4.5 kg).

H-0/144-00 Console drive; 115	VAC, 50/60	Hz\$676.00	)
H-07144-02 Console drive; 230	VAC, 50/60	Hz\$676.00	ļ

# DRIVES FOR MICROPUMP

### PRO-SPENSE™ DIGITAL PUMP/CONTROLLER



Automate your lab systems

with our versatile Pro-Spense" digital pump/controller. Controller can be used with the MICROPUMP pump heads with standard canister (series B and D sold on facing page). Built-in software lets you use controllers to operate pumps, motors, relays, and other devices as you dispense. Convenient LCD keeps you constantly informed of operating conditions. A serial output lets you daisy chain controllers for a number of applications. Connect to analog devices such as pH or flow controllers for precise liquid batch dispensing, or top-loading balances for gravimetric batching or dispensing.

Controller allows you to pump fluids at flow rates up to 4400 ml/min. Max differential pressure is 50 psi; max temperature is 250°F (121°C). Motor speed range is 0-4000 rpm. Measures 51/2" W x 81/2"H x 10"D.

Interface controller with an IBM®-compatible personal computer to download stored programs at any time. Your computer keyboard can also serve as a central control for all pump functions. IBM-compatible software program (included) confirms that proper RS-232 serial connection to your computer has been established. Order connecting cables from the table below.

H-78200-22 Pump/controller; 120 VAC, 60 Hz.	
Shpg wt 10 lbs (4.5 kg)	\$2120.00
H-78200-27 Pump/controller; 240 VAC,	
50 Hz. Shpg wt 10 lbs (4.5 kg)	\$2120.00

### **CONNECTING CABLES**

Cat. no.	Function	Length	Price						
Personal computer and balance cables; DB9 female connector									
H-78200-50 H-78200-52 H-78200-70 H-78200-72 H-78200-74	5 ft 5 ft 6 ft 6 ft 6 ft	\$ 75.50 118.00 59.00 116.00 141.00							
I/O and mast	er/stave cables; DB37 male connector								
H-78200-62 H-78200-64 H-78200-66 H-78200-68	Synchronize 2 pumps; ½" mini jack Synchronize 3 pumps; two ½" mini jacks Interface up to 3 analog units; 3 pigtail leads Access up to 4 TTL switches; 4 pigtail leads	6 ft 6 ft 9 ft 9 ft	65.00 100.00 65.00 59.00						
Autosampler	Autosampler cable; DB15 male connector								
H-78200-54	Interface controller with an autosampler	5.ft	75 50						

ACCESSORIES (for Pro-Spense pump/controllers)

H-78200-58 I/O adapter module. Lets you interface with external devices without inconvenient hookup to the controller's back panel ......\$388.00 H-78200-80 Foot switch allows hands-free operation. Includes 7-ft connecting cord; 1/4" mini jack ......\$82.50

> Cole-Parmer International Fax: 708-549-1700

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# MP HEADS

# °OLE-PARMER® DIGITAL CONTROLLER/DISPENSERS

Feature copy and dispense functions



These versatile new gear pump controller/dispensers accept any MICROPUMP<sup>™</sup> pump head with a standard canister (series B or D sold below). Feature prime, calibrate, dispense, and copy nodes for accurate batching. Continuous-duty systems produce flow rates to 3900 ml/min; accurately dispense from 3 ml to 999 liters (speed control is  $\pm 0.3\%$ ). Systems have remote capabilities through a contact closure—useful for small-scale process applications such as fermentaion and filtration.

Calibration values for 30 different MICROPUMP pump heads are stored and protected in the nonvolatile memory. You can also calibrate controller/dispenser for fluids other than water. Simply press the CAL button, let the pump run for a predetermined amount of time, then enter the correct volume of fluid dispensed. Maximum operating temperature is 104°F (40°C).

The vacuum fluorescent display can be read from a distance of 12 feet. Display indicates volume (ml, i, or oz) or flow rate (ml/min, i/min, or oz/min). Select from models with either a benchtop controller or a NEMA Type 13 wall-mount controller. All systems come with a 180-3600 rpm, NEMA Type 4X "washdown" motor (IP56 rating). Shpg wt 10 lbs (4.5 kg).

### BENCHTOP CONTROLLER

Membrane keypad is sloped for easy access. Controller has a ¼" phone jack for remote start-up using optional foot switch 07595-35 (order at right). A 6-ft cable connects the motor and controlier. Model 75210-00 includes a 6-ft modular line cord with U.S. plug. Model 75210-05 includes a 6-ft modular line cord with IEC 320/CEE 22 connector—please specify country of destination to obtain correct line cord. Both models have an IP43 rating; measure 9"W x 9¼"H x 5"D.

### NEMA TYPE 13 WALL-MOUNT CONTROLLER

Wall mount this controller in your lab or plant. Make all connections to the front-panel terminal strp-controller's transparent cover is hinged for easy access to the controls. You can also operate the system remotely using optional hand-held remote controller 07592-80 (sold separately at right). A 24-ft cable connects the motor and controller. Both the 115 and 230 VAC models come with a 6-ft integral line cord (115 VAC model comes with U.S. three-prong plug; 230 VAC model comes with European plug). Both models have an IP55 rating and measure 10"W x 8"H x 6"D.



### ORDERING INFORMATION FOR CONTROLLER/DISPENSERS

Catalog number	Power	Price	
Benchtop mot	lels		
H-75210-00 H-75210-05	115 VAC, 50/60 Hz 230 VAC, 50/60 Hz	\$1300.00 1300.00	
HEMA Type 13	wall-mount models		
H-75210-10 H-75210-15	115 VAC, 50/60 Hz 230 VAC, 50/60 Hz	1530.00 1530.00	

### ACCESSORIES

H-07595-35 Foot switch for start/stop remote control of benchtop system ......\$70.50 H-07592-80 Hand-held remote controller for use with NEMA Type 13 system. Features start/stop, reverse, momentary on (prime), 

IBM---Reg TM International Business Machines Corp. IBM—Reg TM International Business Machines of Masterflex—Reg TM Cole-Parmer Instrument Co. Pro-Spense—TM Cole-Parmer Instrument Co. MICROPUMP—Reg TM Micropump Corp. Ohaus—Reg TM Ohaus Scale Corp. Ryton-Reg TM Phillips Petroleum Co. Tefton, Viton-Reg TM E. I. du Pont de Nemours & Co.

							(					Service	kit
i'u	uno heads*	Max flow	(ml/min)	Max pres	sure (psi)	Materials c	t construct		Temperature	Bypass	Price	Catalog	Price
Series	Catalog number	Cole- Parmer'	Pro- Spense'	System	Diff	Body	Gears**	Seals	range	valve		number	
	style partic bear	ic with stor	idard cum	stor			Tellon	Teflon	-50 to 130°E'	No	\$405.00	H-07144-38	\$136.00
В	H-07002-16 H-07002-17	1140 1140	1260 1260	300 300	45 45	316 SS 316 SS	Teflon	Teflon	-50 to 130°F"	Yes	405.00 373.00	H-07144-38 H-07002-08	136.00 84.50
В	H-07002-23	2300	2600	300	45	316.55	Byton	Teflon	-50 to 250°F	Yes	373.00	H-07001-89	84.50
В	H-07001-80	2300	2600	300	45	Ditop/316 SS	Byton	Teflon	-50 to 250°F	Yes	267.00	-	
В	H-07001-70	2400	2700	300	45	216 55	Teflon	Teflon	-50 to 210°F	No	373.00	H-07001-41	84.50
В	H-07001-40	3400	3800	300	45	310 33	Tenen	1					
D	H-07002-25	neads with 60 150	70 70 170	i canister 300 300	50 50	316 SS 316 SS	Teflon Teflon	Teflon Teflon	-50 to 130°F' -50 to 130°F' -50 to 130°F	1 No 1 No 1 No	419.00 419.00 419.00	H-07144-42 H-07144-44 H-07144-47	141.00 141.00 141.00
D	H-07002-27	300	335	300	50	316.55	Duton	Teflon	-50 to 210°F	No	419.00	H-07144-34	141.00
D	H-07002-14	330	370	300	50	316 55	Tefler	Teflon	-50 to 210°F	Yes	392.00	H-07003-12	101.00
D	H-07003-02	2000	2300	300	50	316 55	Buton	Viton	-50 to 250°F	No	392.00	H-07003-14	101.00
	H-07003-04	3900	4400	300	45	Hyton/316 SS	nyton	1 1101	water with po hac	k pressure	at 3600 rpm.		

"For complete information on these pump heads and service kits, see pages 1130-1131. "Nominal flow rate p Nominal flow rate pumping water with no back pressure at 4000 rpm. "Port size for all models is 1/6" NPT(F). 'Nominal flow rate pumping water with no back pressure at 3000 rpm. nodels is 1/4" NPT(F). "Up to 210°F using the high-temperature seals 07002-05 on page 1130.

# PUMPS



Positive displacement: Gear

# Smalec VARIABLE-SPEED DRIVES

# STANDARD DIGITAL DRIVE

- Pulseless flow from 0.3 to 6650 ml/min
- 🖪 Numeric speed adjustment
- Remote control capability

This standard variable-speed drive accepts any MICROPUMP® pump head with standard canister (series B and D). Select pump heads and service kits from the table at the bottom of the facing page.

Precisely control speed from 70 to 6100 rpm with an accuracy of  $\pm 1\%$  of setting over full range. Electronic feedback system compensates for changes in load. Tach-generator on motor shaft produces a 0-7 VDC output signal for remote indication of motor rpm.

Use the three-digit potentiometer to set pump speed from 0.1 to 99.9%. **NOTE:** Avoid running drive continuously at less than 20% or more than 85% of full speed. Press the "max" button for extra rpm; ideal for quick pump priming.

Control input port (DB15 female connection) lets you use peripheral instruments to actuate many of the drive functions from a remote location (remote cable required). Use a remote controller (with NO contact) to turn the pump on and off; use an external control signal (0-4.7 VDC, 0-10 VDC, 0-20 mA, or 4-20 mA) to vary pump speed.

Permanent-magnet DC motor provides smooth acceleration. Motor magnetically couples to pump head so there are no shaft seals to wear out or leak. Drive housing measures  $9\frac{1}{2}W \times 6\frac{1}{10} \times 7\frac{13}{16}$ "D. Both the 110 and 220 VAC models include a 6-ft power cord with U.S. standard plug. Order drive and remote cable from the table on the facing page.

# NEW PROGRAMMABLE DIGITAL DRIVE

- T LED display indicates flow rate
- Built-in RS-232-C interface and optional software let you automate pumping processes

Choose this new programmable digital drive for versatility! Drive offers the same features as the standard digital drive at left plus the advantages of a built-in RS-232-C interface. Order RS-232-C interface cable 78098-50 separately below to connect drive to any IBM\* PC/XT/AT\* or 100% compatible computer. You can also use the optional software with additional cables to control up to eight drives simultaneously!

Front-panel keypad lets you set all operating parameters including pump speed (1-6100 rpm) and dispensing mode. The 4-digit LED with adjustable scale indicates flow rate or drive rpm. Use drive for continuous pumping or select one of the three dispensing modes for added convenience. Use the time mode to set dispense and pause times. The step mode lets you set the number of shaft rotations for precise dispensing. Use the valve mode to control an external diverter valve (not included) for dispensing two liquids in the same batch. You can even use all three modes simultaneously for maximum versatility and dispensing accuracy.

Control pump speed remotely via an analog input signal (0-4.7 VDC, 0-10 VDC, 4-20 mA, or 0-20 mA); start and stop flow remotely via contact closures. Make all remote control connections via the back panel DB15 female connector. Tachometer output sends a voltage signal (0-7 or 0-4.35 VDC) proportional to drive speed. Or, order optional software 78002-99 (sold below) to control all drive functions including calibration, ramp and on/off times, and fluid direction.

Drive measures 6"W x 10%"H x 8½"D: includes a 5-ft cord with U.S. standard plug. Operates on 110/220 VAC, 50/60 Hz (switch selec-table). Order drive from table on facing page.





# PUMPS



Positive displacement: Gear

# **COMPACT DRIVES**

Flow from 0.1 to 4700 ml/min

Ģ

Use these space saving, variable-speed drives with MICROPUMP pump heads with standard canister (series B and D except models 07003-02 and -04). Each compact drive comes with adapter plate

Adjust speed with the 10-turn potentiometer—get linear speed regula-tion from 50 to 5000 rpm with an accuracy of  $\pm 1\%$  over the full range. **NOTE:** Avoid running drives continuously at less than 20% or more

Five-pin remote-input port on back panel accepts a 0-4.7 VDC, 0-10

contact for on/off control (order remote cable from table at right). Choose either an integrated drive or a modular drive. The integrated drive measures just 7¾"L x 5"W x 3¾"H. The modular drive connects to a remote speed controller via a 6-ft cord (drive measures  $6^{4}$ "L x  $2^{1}$ "W x  $3^{1}$ "H; controller measures  $7^{4}$ "L x  $5^{1}$ W x  $3^{4}$ "H). Both the integrated and the modular drives are available in 110 and 220 VAC versions; include a 6-ft power cord with U.S. standard plug

VDC, 0-20 mA, or 4-20 mA signal for speed control; couples with relay

H-07617-90 Replacement adapter plate for mounting MICROPUMP

series B and D pump heads (except models 07003-02 and -04) on

Remote control capability

Compact

integrated drive 07617-60 shown with series B pump head

07617-90 for mounting pump head.

than 85% of full speed.

Compact, unmounted drive 07617-75 with remote speed controller— shown with series B pump head



pump head adapter plate 07617-90.

### **ORDERING INFORMATION FOR DRIVES**

Catalog	Power	Shpa wt	_ ·	Remote a	able
number	VAC, Hz	lbs (kg)	Price	Cat. no.	Price
Siandara digit	al drive				
H-07617-70 H-07617-72	110, 60 220, 50	19 (8.6) 19 (8.6)	\$2060.00 2060.00	H-07339-50	\$136.00
Programmabi	c digital driv	ve			
H-78004-00	<b>78004-00</b> 115/230, 50/60		2820.00	·	
Compact into	grated drive	ż			
H-07617-60 H-07617-62	110, 60 220, 50	7 (3.2) 7 (3.2)	1390.00 1500.00	H-07339-54	82.50
Compact mod	inar drive a	and control	er		
H-07617-75 H-07617-77	110, 60 220, 50	6 (2.7) 6 (2.7)	1590.00 1590.00	H-07339-54	82.50



# SPECIFICATIONS AND ORDERING INFORMATION FOR MICROPUMP® PUMP HEADS

David Land 1		May flow	(mt/min)	May pres	sure (nsi)	Materials	of construction		Temperature	Bypass	SS Deine	Service kit	
Pu	Catino	Digital	Compact	System	Diff	Body	Gears <sup>†</sup>	Seals	range	valve	Price	Cat. no.	Price
Series	<u> </u>	L valuer					·4						
B B B	H-07002-16 H-07002-17 H-07002-23	1950 1950 1950 3900	1580 1580 3200	300 300 300	45 45 45	316 SS 316 SS 316 SS	Teflon® Teflon Teflon	Teflon Teflon Teflon	-50 to 130°F <sup>4</sup> -50 to 130°F <sup>4</sup> -50 to 130°F <sup>4</sup>	No Yes Yes	\$405.00 405.00 373.00	H-07144-38 H-07144-38 H-07002-08	\$136.00 136.00 84.50
BB	H-07001-80 H-07001-40	3900 5730	3200 4700	300 300	45 45	316 SS 316 SS	Ryton* Ryton	Teflon Teflon	-50 to 250°F -50 to 210°F	Yes Yes	373.00 373.00	H-07001-89 H-07001-41	84.50 84.50
Pr	re-basice pone	heads via	naciadard	Caibaut								·····	
D	H-07002-25 H-07002-26	104 250 510	85 210 420	300 300 300	50 50 50	316 SS 316 SS 316 SS	Teflon Teflon Teflon	Teflon Teflon Teflon	-50 to 130°F <sup>†</sup> -50 to 130°F <sup>‡</sup> -50 to 130°F <sup>‡</sup>	No Yes Yes	419.00 419.00 419.00	H-07144-42 H-07144-44 H-07144-47	141.00 141.00 141.00
	H-07002-27	560	460	300	50	316 SS	Rvton	Teflon	-50 to 210°F	Yes	419.00	H-07144-34	141.00
	H-07002-14	2440	400	300	50	316 SS	Tefion	Teflon	-50 to 210°F	Yes	392.00	H-07003-12	101.00
	H-07003-02	6650		300	45	Rvton/316 SS	Ryton	Viton <sup>®</sup>	-50 to 250°F	Yes	392.00	H-07003-14	101.00
	n-0/003-04	0000				in the Dort	izo for all m	odele je 1/4"	NPT/E) <sup>1</sup> Tem		n to 210°F ca	n be reached using	optional hig

See pages 1130-1131 for complete information on these pump heads and service kits. temperature seals 07002-05 on page 1130. MICROPUMP---Reg TM Micropump Corp.

Ryton-Reg TM Phillips Petroleum Co.

Teflon, Viton-Reg TM E. I. du Pont de Nemours & Co.





IEC/ISO 71 drives.Includes hub assembly (drive magnet), hex key, mounting bolts, and mounting plate. Shpg wt 3 lbs (1.4 kg) ....\$228.00 H-07003-98 IEC 72/ISO 63 pump head adapter kit for IEC/ISO 63 drives. Includes hub assembly (drive magnet), hex key,

mounting bolts, and mounting plate. Shpg wt 3 lbs (1.4 kg) .... \$228.00

H-07003-99 NEMA Type 56 C-face pump head

adapter kit for 3450 rpm, 56 C-face drives. Includes metal adapter, hub assembly (drive magnet), mounting screws and bolts, and an H-07002-15 MICROPUMP pump head adapter

for 600 rpm Masterflex\* L/S drives ......\$144.00

# MOTORS FOR MICROPUMP® PUMP HEADS WITH LARGE CANISTER

Motor 07003-36 shown with pump head 07003-30 Combine these powerful motors with MICROPUMP pump heads with large canister (series E and G) for high-torque, continuous-duty pumping. Use the table directly below to determine the best combination of pump head and motor for your desired flow rate. Order pump heads from the first table; order motors from the second table.

See page 1132 for a full description of MICROPUMP series E and G pump heads with large canister (sold below) and pump heads with 56 C-face flange adapters.

# SPECIFICATIONS AND ORDERING INFORMATION FOR MICROPUMP® PUMP HEADS

E Pu	unn heads	Max flow	dia and the tax							
Series	Cat	Max now	(liters/min)	using indica	ated pump	motor		Service	Service kits	
Genes		07002-51, -49	07003-36	07003-37	07003-83	07003-82	Price	Cat no	Drice	
E	H-07001-92 H-07001-94		5.4	5.4	5.4	5.5	\$3680.00		-nce	
G	H-07003-06	3.0	10.9	10.9	10.9	11.3	4220.00			
G	H-07003-08	5.4	_	_	_	_	816.00	H-07003-16	\$114.00	
G	H-07003-30		5.5	4.5	5.5*	7.41	010.00	H-0/003-18	114.00	
G	H-07003-31		11.3	9.0	11.3*	14.9 <sup>1</sup>	855.00	H-07003-38 H-07003-39	114.00	

mum intermittent pressure may be lower in these pump head/motor combinations These pump head/motor combinations require 40 psi air to inlet pressure

# SPECIFICATIONS AND ORDERING INFORMATION FOR MOTORS

	Cat. no.	Туре	rpm	Motor	hn	Power power				
	H-07002-51	AC	3400	TEEC/PSC	0.125		Iermination	Dimensions	Shpg wt	Price
	H-07003-36 H-07003-37	AC AC	3200 3200	TEFC/PSC TEFC/PSC	0.250	115 VAC, 50/60 Hz, 2.1 A 115 VAC, 50/60 Hz, 3.0 A 230 VAC, 50 Hz, 1.5 A	14" wire leads 15" wire leads	7½"L x 4¾"W x 5¾"H 7½"L x 4¾"W x 5½"H	9 lbs (4.1 kg) 10 lbs (4.5 kg)	\$340.00
	H-07002-49 H-07003-83 H-07003-82	AC AC Air	3150 3150	XPRF/PSC XPRF/PSC	0.170 0.170	115/230 VAC, 50/60 Hz, 1.8 A 115/230 VAC, 50/60 Hz, 2.2 A	6" wire leads 6" wire leads 6" wire leads	7½"L x 4¾"W x 5½"H 12½"L x 4¾"W x 5½"H 12½"L x 4¾"W x 5¼"H	10 lbs (4.5 kg) 25 lbs (11.3 kg)	340.00 634.00
N	fasterflex—Reg Tr	M Cole-P	armer Ins	trument Co.	MICROPU	10 to 16 SCFM, 20 to 60 psi IMP-Reg TM Micropump Corp.	1/4-28 UNF	8¾"L x 4¾"W x 6"H	20 lbs (9.1 kg) 7 lbs (3.2 kg)	634.00 653.00

1138

#### **Cole-Parmer International** Fax: 708-549-1700

Motor 07002-49 shown with pump head 07003-06

فتعاطيه بعلالته المتلا With the all a strating and the second second second second فالملاط فللطاف والناد المنافق

14414 Martin 101- 101100

# TUTHILL MAGNET DRIVE GEAR PUMPS



**D-SERIES** Stainless Steel Seal-less Hi-Torque Magnet Drive Gear Pumps

Flow Rates to 2 GPM Temperatures to 350° F





- Chemical Handling
- Oil Filtration

UN 15:25 FAA

- Negative Pressure
- Solvent Handling
- Instrumentation Cooling
- Pilot Plant
- Sampling
- Proportioning
- Laboratory
- Refrigerant Recycling
- Additive Delivery
- Seal Flush
- Fluid Transfer
- Spraying

# STANDARD PUMPHEAD SPECIFICATIONS

- 30 in oz Magnetic Coupling
- Pump Body, Cavity Plate & End Cap 316 Stainless Steel, Hastelloy or Titanium Available
- Gears -- Nickel Alloy Driving, Carbon/Teflon filled Ryton Driven
- Gear Shafts 316 Stainless Steel
- Bearings Carbon/Teflon filled Ryton
- By-Pass/Pressure Relief Externally Adjustable
- O-Rings Virgin Teflon
- Driven Magnet Barium Ferrite
- Magnet Cup 316 Stainless Steel
- 1/8 N P T Straight Through Porting (1/4 N P T and other ports Available)
- System Pressure 500 PSIG

"LEAK-FREE MAGNET DRIVE MAKES THE DIFFERENCE."



TuthIII Pump Co. of California

5143 Port Chicago Highway Concord, California USA 94520 Tel 510 676-6000 Fax 510 676-6151

Page 4

# **D SERIES** — PUMP AND MOTOR SELECTION GUIDE **30 INCH OUNCE MAGNETIC TORQUE**

# MODEL NUMBER = PUMPHEAD + MOTOR & DRIVE

4.38 x 4.00 x 9.50

7,5 lbs.

### PUMP PERFORMANCE CURVES VARIOUS GEAR WIDTHS AND MOTORS - 77°F WATER



Page	5

20 lbs,

20 lbs.

5.25 x 5.00 x 15.25

5.25 x 5.00 x 15.25

D 9863 MC - D 5676

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### **APPENDIX 4**

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# MASS FLOW AND PRESSURE MEASUREMENT AND CONTROL















GERITIFIED (SO-900) INNIOVATITUE WIDE PRODUCT RANGE REHABLE GLOBAL SERVICE







# LIQUI-FLOW MASS FLOW METERS/CONTROLLERS

### 🖝 GENERAL

The LIQUI-FLOW series thermal mass flow meters/controllers for liquids are suitable for measuring flows of 0...5 g/h up to 0...1000 g/h, at pressures from vacuum up to 400 bar.

The flow meter is basically an obstructionless tube with an internal diameter of 1 mm, bent in U-form, with patented heater/sensor. In the sensor, the liquid gets merely 1 degree warmer than the environmental temperature, so that the chance that the liquid will decompose or gas-out is negligible.

The instrument has a "thru-flow" measuring principle and it is insensitive to its mounting position. Moreover, the flowmeter can be sterilized and does not

contain any moving parts or elastomer seals. The LIQUI-FLOW meter has an integrated control function and can be connected to a COMBI-FLOW control valve to form a control loop. The control valve with standard purge connection on the top of the sleeve takes care of steady flow control, not pulsating, even when controlling flows lower than 1 g/h.

- APPLICATIONS IN
- Pharmaceutical industry
- Food industry
- Biotechnical industry
- Analytical laboratories
- Semiconductor industry
- Evaporation processes (see page 15)







THERMOPILE WITH APPROX. 5000 THERMOELEMENTS

#### FEATURES

- Thru-Flow measurement
- 1°C temperature rise in sensor
- Superstable zero
- Attitude insensitive
- Wide flow ranges 1:50
- Sterilizable
- Orbitally welded
- Metal sealed

### FLOW CAPACITIES (BASED ON WATER)

Mass Flow Meters:

Series L1:	min.	0,15	g/h
	max.	2100	g/h
Series L2:	min.	2100	g/h
	max.	201000	g/h
Mass Flow Controllers:			
Series L1C2:	min.	0,15	g/h
	max.	$2 \dots 100$	g/h
Series L2C2:	min.	2100	g/h
	max.	$20 \dots 1000$	g/h

# POWER SUPPLY/READOUT SYSTEMS

**DIGITAL SINGLE CHANNEL MODULE; SERIES E-7000** Bronkhorst High-Tech B.V. offers the Digital Single Channel Control Module for use with Thermal Mass Flow Controllers, Electronic Pressure Controllers and other transmitters and transducers or, as in master/slave control systems, in combination with these.

The Bronkhorst Hi-Tec E-7000 Series FLOW-BUS is designed to easily enable the user through a menu format to program and power one meter or controller.

The micro-processor based unit offers great flexibility in indication of tags, fluid names and counter units in combination with measuring and setpoint values, both in percentages or actual units.

Furthermore the polynominal function of the calibration curve, offering an accuracy of  $\pm 0.5\%$  off reading plus  $\pm 0.1\%$  full scale, can be stored.



E-7100 3-CHANNEL EXECUTION

### MULTI-CHANNEL EXECUTIONS; SERIES E-7000

Based on the modular technique of the single channel modules, it is easy to assemble multi-channel executions. This way 3 channels fit into a 1/2 19" housing and 6 channels fit into a 19" housing, either for rack mount or table top.



A user friendly readout/control/alarm/totalization module; supply voltage 100...240 Vac, 24 Vac or 24 Vdc; with 5-key push-button menu format for:

- operation with digital or analog instruments
- direct or percentage reading
- internal or external setpoint mode
- master/slave control mode
- totalizer/batchcounter function
- one programmable alarm function
- one NO/NC relay
- storage of polynominal calibration function
- CE certification



# POWER SUPPLY/READOUT SYSTEMS

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E-7100 3-CHANNEL EXECUTION

### 57 MULTI-CHANNEL EXECUTIONS; SERIES E-7000

Based on the modular technique of the single channel modules, it is easy to assemble multi-channel executions. This way 3 channels fit into a 1/2 19" housing and 6 channels fit into a 19" housing, either for rack mount or table top.

### FEATURES

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A user friendly readout/control/alarm/totalization module; supply voltage 100...240 Vac, 24 Vac or 24 Vdc; with 5-key push-button menu format for:

- operation with digital or analog instruments
- direct or percentage reading
- internal or external setpoint mode
- master/slave control mode
- totalizer/batchcounter function
- one programmable alarm function
- one NO/NC relay
- storage of polynominal calibration function
- CE certification



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**APPENDIX 5** 

.

# BIOENGINEERING

Doc no. 1220-05a TB, Reg.6

1 (2)

# Wägezelle Load cell

### 1kN.....500kN

Die Wägezelle, bestehend aus Messzelle, Bodenplate mit Halteblock und oberes Joch, misst die Scherkraft und ist weitgehend unbeinflusst, wo die Last im aktiven Teil aufliegt. Es sind keine zusätzlichen Befestigungen oder Querlenker erforderlich. Eine Abhebesicherung (unteres Joch) ist als Option erhältlich.

#### wichtige Merkmale

- hohe Genauigkeit und Reproduzierbarkeit
- Keine Falschmessung bei Temperaturausdehnung der Konstruktion
- Gegen Vibration unempfindlich
- Querkräfte haben keinen Einfluss
- einfache Montage

The load cell consisting of measuring cell, base plate, fixing block and yoke measures the shear force. It is practically irrelevant where or how the actual load is distributed on the cells. Additional fixations or guides are not necessary. For additional safety to prevent any lift offs the lower yoke optional can be used.

important characteristics

- high precision- and reproducibility
- no faulty readings because of expansion of the construction due to temperature changes
- insensible to fibrations
- cross force do not influence the measuring result
- easy installation



#### Bodenplatte Messzelle

c oberes Joch

а

b

- unteres Joch
- (Option)
- F1 Krafteinleitungspunkt, auf Zylinder verschiebbar
- F2 Querkraft kann bis 100% des Messbereiches ausmachen

#### base plate measuring cell upper yoke lower yoke (optional)

force absorbtion on the cylinder shiftable

cross force can be up to 100% of the measuring range

# Anwendungsbeispiele / application examples



Wägezelle unter Beinstütze montiert

load cell under , feet



Wägezelle im Behältersockel eingebaut

load cell installed in pedestal



Wägezelle unter Aufhängevorrichtung montiert

load cell on vessel suspension system



Standardanordnung bei Behälterwagen. Die Wägezellen werden sternförmig angebracht. Dadurch ist der Behälter autom. festgehalten.

basic arrangement for load cells installed evenly distributed to hold the vessel firmly in place.

Doc no. 1220-05a TB, Reg.6

ł

2

1kN.....500kN





Typ A weist eine höhere Genauigkeit auf als Typ B. Der Zylinder ist horizontal einfach zu de/montieren.

Type A has a higher precision and the cylinder is easely mounted/demounted horizontally.

Турс	: kN*	ka**	Liter/litra***			_				•
Δ	1	200	encipatie	A	В	C	D	E	F	Art. No.
<u>^</u>		300	150	175	75	151	51	35	81	50940
<u>A</u>	2	600	150300	175	75	151	51	26	01	50040
<u>B</u>	5	1500	400750 1	205	110	170			81	50941
B	10		1000 1500 1	205	110	175	80	40	110	50942
R	20	6000		205	110		80	40	110	50943
0			200030001	205	110	175	80	40	110	50944
<u>0</u>	50	15000	<u>450010000 I</u>	260	150	230	115	0.3	140	50045
<u>B</u>	100	30000	1200018000 [	300	180	260	124	00	149	50945
В	200	60000	20000 30000 1	240	100	200	134	60	172,5	50946
A	500	150000			200	290 .	160	60	206	50947
•		150000	1	-	-	-	-	_	_	50948
	Nennkrat	von 1 Wägezell	• •	rated load of 1	load cell					0
•••	max. Wag	evereich von 3 V	Vägezellen ** i	max. measuring	range of 3	load cells				
	rer mente	100217								

\*\*\* Fermenterinhalt

... fermenter volume .

Technische Daten	Technical data	<b>T</b> •	•
Nennkraft	rated load	Туре А	Туре В
Genauigkeit		<u>1kN, 2kN</u>	5200kN
Penroduzioshavlasia	precision	0,05%	0.1%
neproduzieroarkeit	repeatability	0.01%	0.0206
zulassige Überlast	overload, safe	1000/	0,02%0
Seitenkraft max.	side load	100%	50%
Werkstoff	motorial	100%	100%
Temperaturbaraiah	material	stainles	ss steel
Medar Namhaft / Medar Historia	temperature range	-40	+100°C

% der Nennkraft / % of rated load

BIOENGINEERING Bioengineering AG, CH-8636 Wald

# Gewichtssonden

zur kontnuierlichen Bestimmung der Flüssigkeitsmenge in Bioreaktoren, Vorlagentanks und drucklosen Behältern

- millimetergenau
- leicht einbaubar in normierten ø25mm-٠ Stutzen
- Elektronikteil (Verstärker) für 4-20 mA-Signal ist im Sensorgehäuse integriert
- Gemessen wird die Flüssigkeitssäule über der Messzelle
- Sondenlänge und Druckaufnehmerempfindlichkeit werden dem Reaktor angepasst
- bestehende Anlagen lassen sich leicht nachrüsten
- temperaturbeständig bis 130 °C

# Weighing probes

for the continuous measurement of liquid volume in bioreactors, storage tanks and non-pressure vessels

- up to the next millimeter
- easy installation in a standard 25mm port
- electronics integrated in the sensor head ٠ part (amplifier) for 4-20mA signal
- the liquid level above the measuring cell is measured
- the length and the sensitivety of the probe are individualy adjusted for each reactor
- existing installations can be easely retrofitted
- temperature resistant up to 130 °C

# Membranventil diaphragm valve Druckaufnehmer 1 pressure probe 1 $\Delta p = p2 - p1$ Druckaufnehmer 2 pressure probe 2 n2

Gewichtssonde für drucklose Behälter Weighing probe for non-pressure vessels



- Druckdifferenz Δp
- p1 atmosphärischer Druck
- p2 hydrostatischer Druck
- vв Vollbereichssignal

- Δp pressure difference
- p1 atmospheric pressure
- hydrostatic pressure p2 vв
- full range signal

Gewichtssonde, sterilisierbar Weighing probe, sterilisable

51250

drucklos/non-pressure



Technische Daten	Technical data					
Betriebstemperatur	operating temperature				max.	130 °C
Werkstoff: Mediumberührte Teile	material: parts in contact with me	dium			1.443	5 (31)
Messprinzip	measurement principle				Piezo	resistiv
Messbereiche bis	measuring range up to	1	2	5	10	m
Überlast (Differenzdruck)	overload (pressure difference)	2.5	2.5	2.5	3	bar
Vollbereichssignal (VB)	full range signal (VB)	80	150	300	400	mV
Linearität	linearity	+1	+3	+10	+24	mm
Repetierbarkeit	repetition	<u>+1</u>	+2	+5	+10	mm
Auflösung	accuracy	<u>+</u> /	<u> </u>		<	10-5 VB
Bestellangaben	details of ordering					Art. No.
Gewichtssonde*, sterilisierbar	weighing probe*, sterilisable					11857
Gewichtssonde* für drucklose Behälter	weighing probe* for non-pressure	vessels	•••••••	·····		11856
Strömungsdämpfende Bodenhülse	flow absorbing hood					44662
O-Ring-Satz	O-ring set		sterilis	ierbar/steril	isable	51251

\* mit Kabel u. Stecker

\* with cable and cable plug

Doc no. 0922-20 TB, Reg.6 1 (1)

# Plattformwaagen Platform scales





Typ A, Wägebereich bis 60 kg type A, measuring range up to 60 kg Typ B, Wägebereich von 300 bis 1250 kg type B, measuring range from 300 to 1250 kg

Type type	Wägebereich measuring range	Dimensionen BxLxH dimensions WxLxH	Auflösung resolution	Fermenter Typ/Grösse fermenter type/size	Art. Nr. Art. no.
<u>A</u>	60 kg	390 x 530 x 120	0,02kg	KLF	51033
B	300 kg	610 x 610 x161	0,1kg	L1523, NLF	51034
<u>B</u>	500 kg	762 x 762 x 161	0,2kg	LP 4275 I	51035
В	1250 kg	1016 x 1016 x 171	0,5kg	P 100300 I	51036

Technische Daten	Technical data			
Gewichtsmesszelle:	load cell:		tyne A	tune B
Widerstand	resistance		3500	2500
Verstärkungsverhältnis	amplification		<u>1 m\//\/</u>	<u> </u>
Exc.	exc.			2 mv/v
Nichtlinearität	non linearity	, <u>, , , , , , , , , , , , , , , ,</u>	0.015%	0.03%
Temperatureffekt	temp. effect	żero	0,004%/°C	±0,15%
		span	0.0014%/°C	+0.08%

Blick auf Stecker			А	В	plug pin
plug plns	Exc.	+	red	white	3/5
3 2	Exc.	-	white	green	4/6
	signal	+	green	red	1
	signal	-	blue	black	2
5001	shield		yellow	orange	7

Steckerbelegung / pin arrangement