

# THE MARSHIAN:

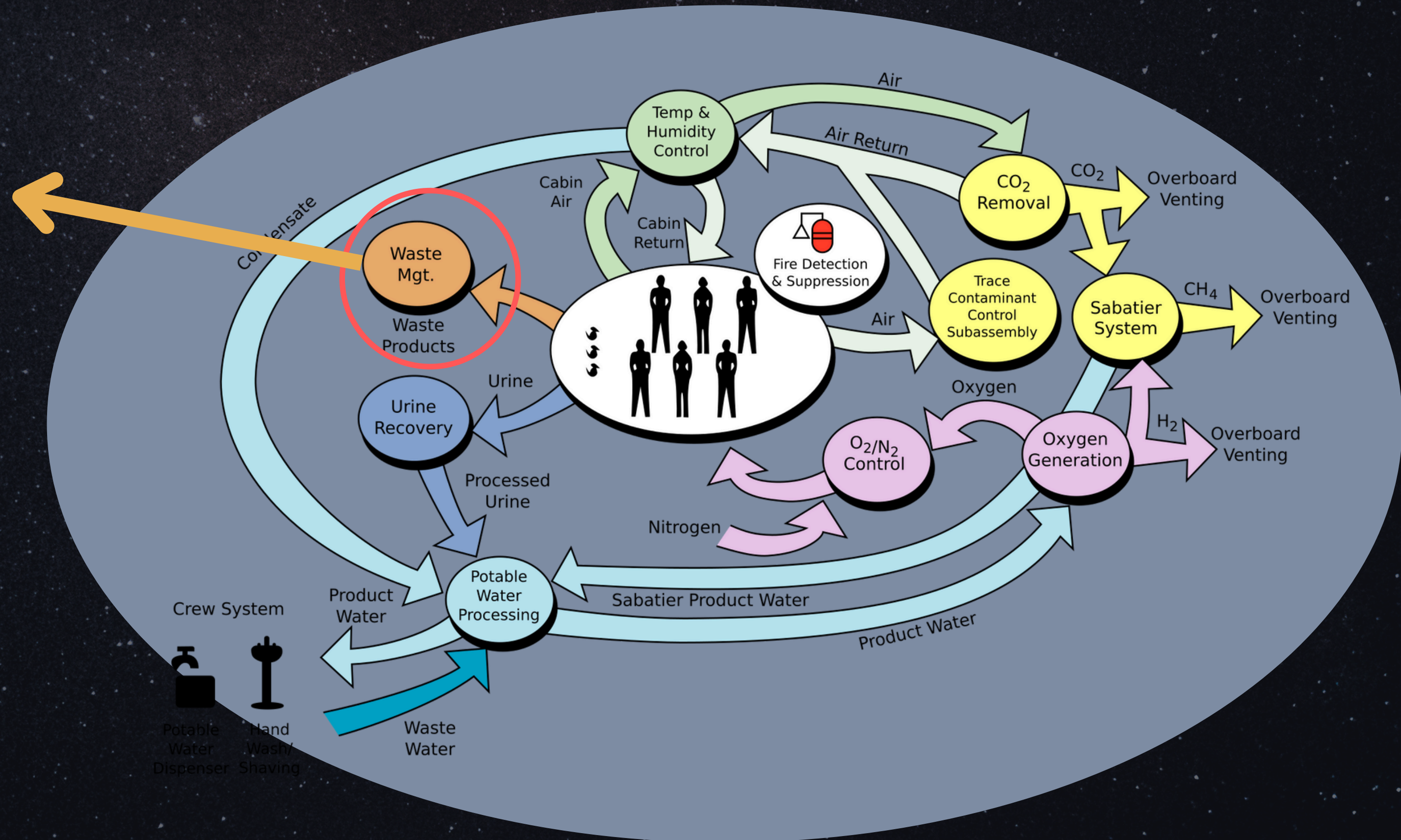
**SIMULATION OF A  
WASTE TREATMENT  
WETLAND FOR THE  
MOON OR MARS**



The Spring Institute for  
Forests on the Moon



# Problem



State of the art ECLSS ignores solid waste.



# Cost of Waste

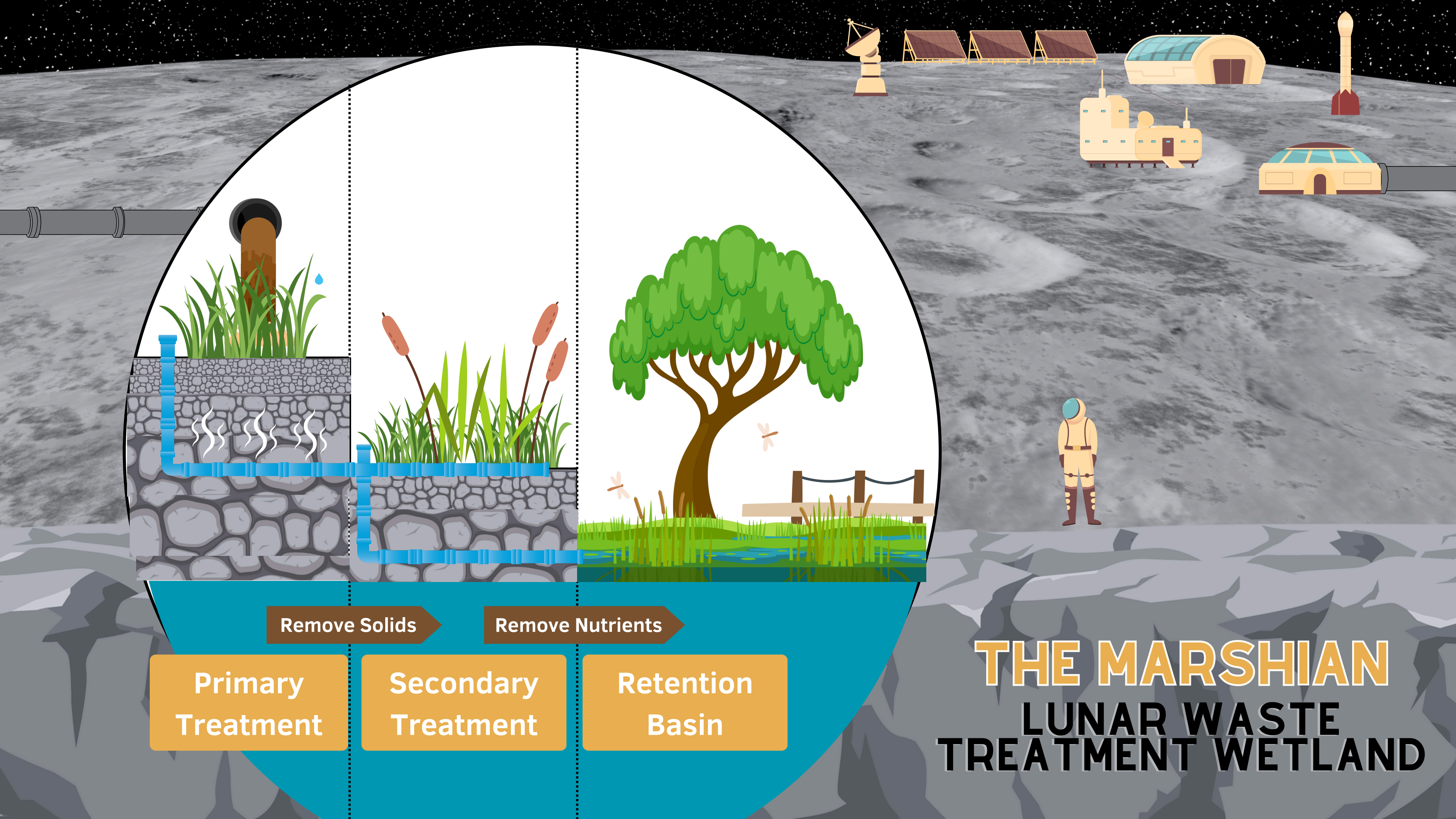
**A HUMAN PRODUCES 128KG OF FECES/YEAR**

With an average of 7 ISS crew at a time, that's 896kg of upmass per year.

896kg to LEO  
@ \$93k/kg =  
**\$83M**

896kg to Lunar Surface  
@ \$1.2M/kg =  
**\$1.1B**





Remove Solids

Remove Nutrients

Primary  
Treatment

Secondary  
Treatment

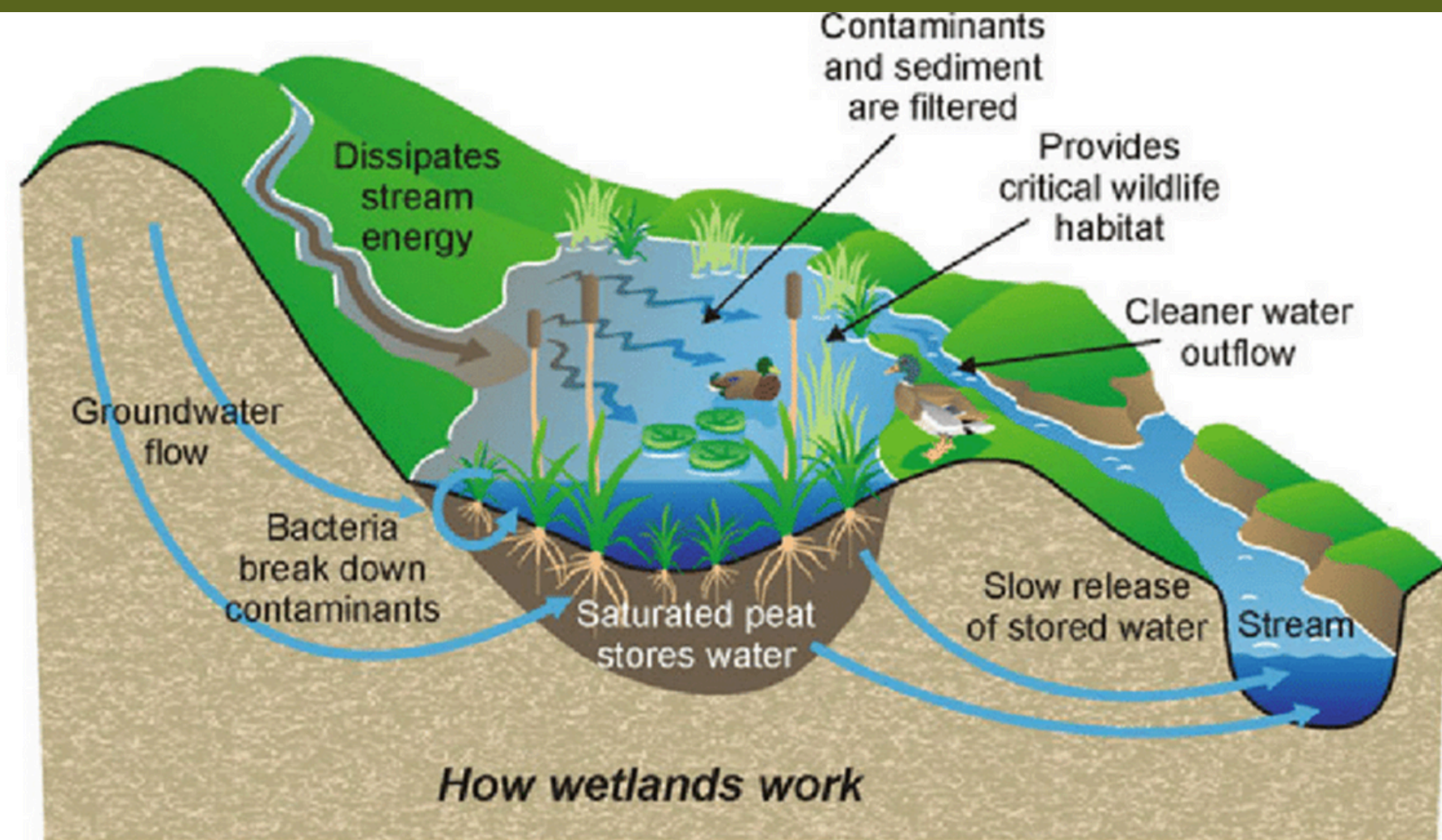
Retention  
Basin

# THE MARSHIAN LUNAR WASTE TREATMENT WETLAND

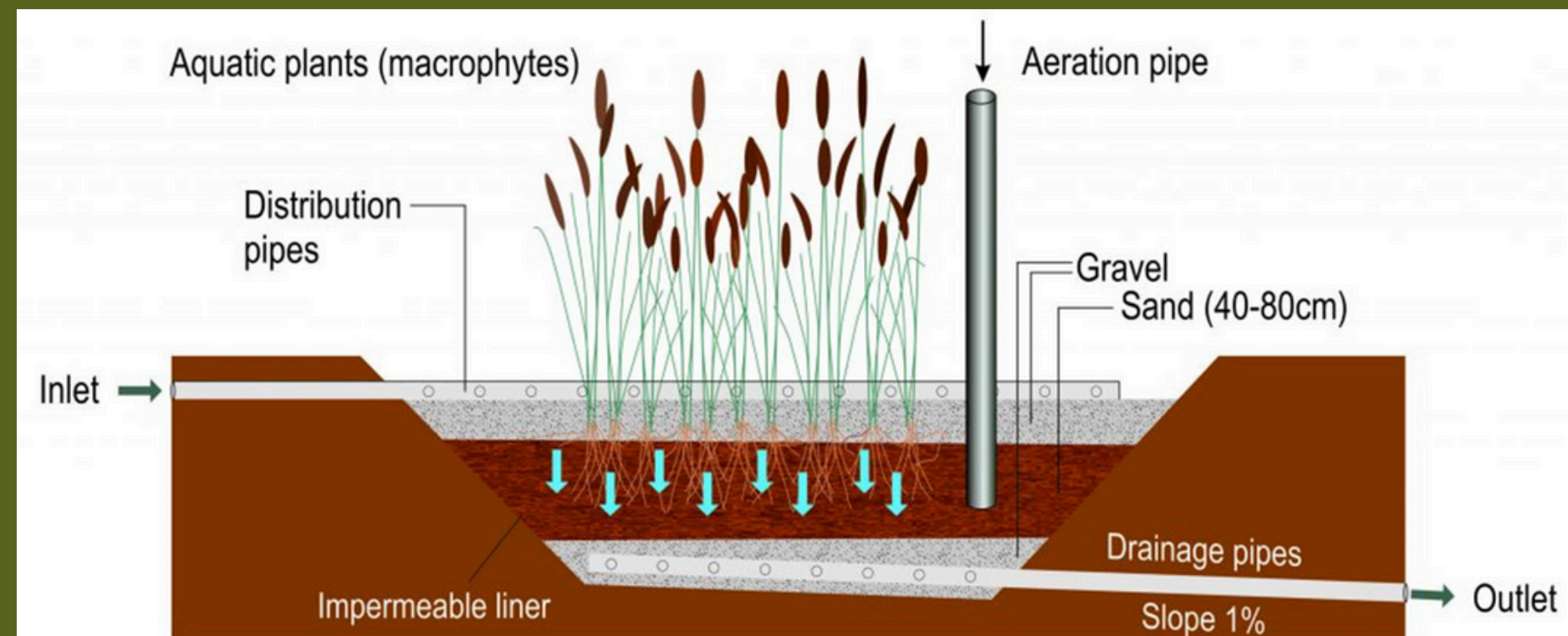


# Wetland Removal Processes

## Natural Wetland



## Artificial/Constructed Wetland





# Simulation Objectives



## Continuous vs Intermittent Operation

Investigate alternative feeding schemes to reduce the required footprint of the system.



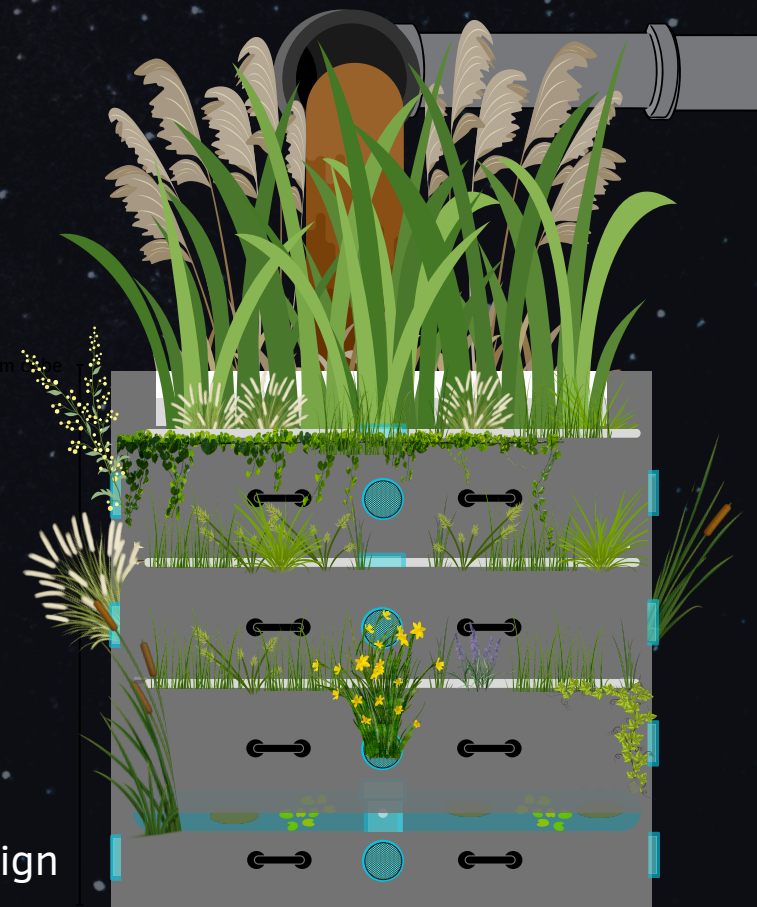
## Effect of Reduced Gravity

Compare performance of the same constructed wetland in Earth gravity and in lunar gravity.



## ISRU Feasibility

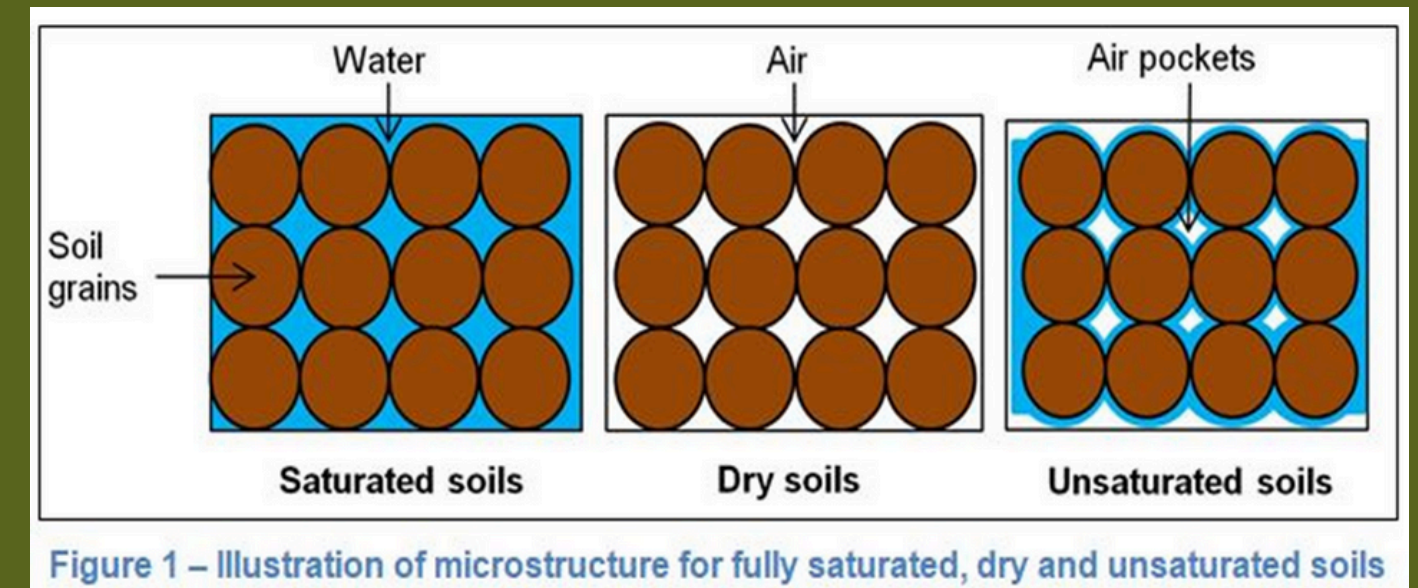
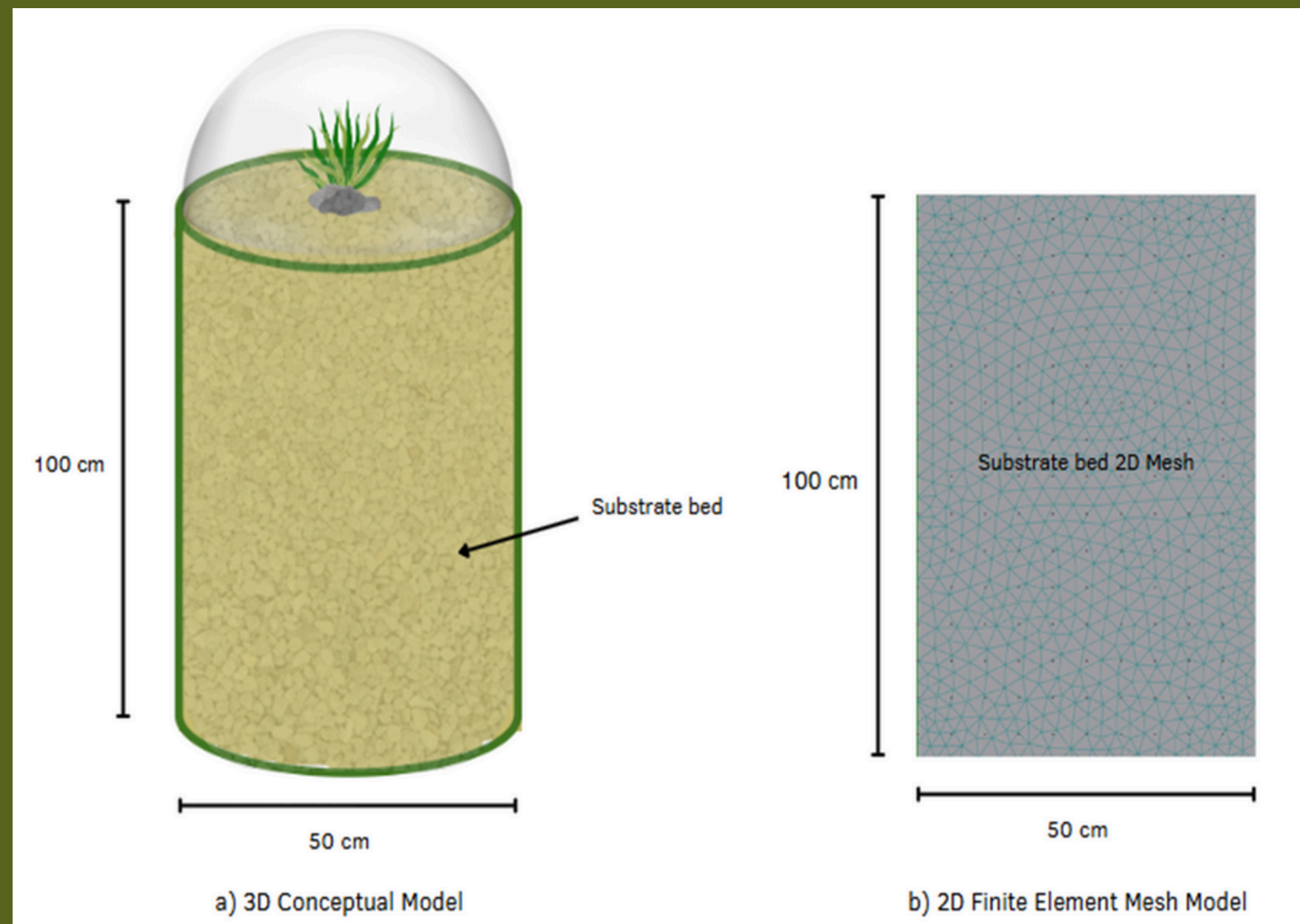
Compare the performance of the same constructed wetland built with conventional sand versus lunar regolith for the reactor bed.



First Conceptual Design



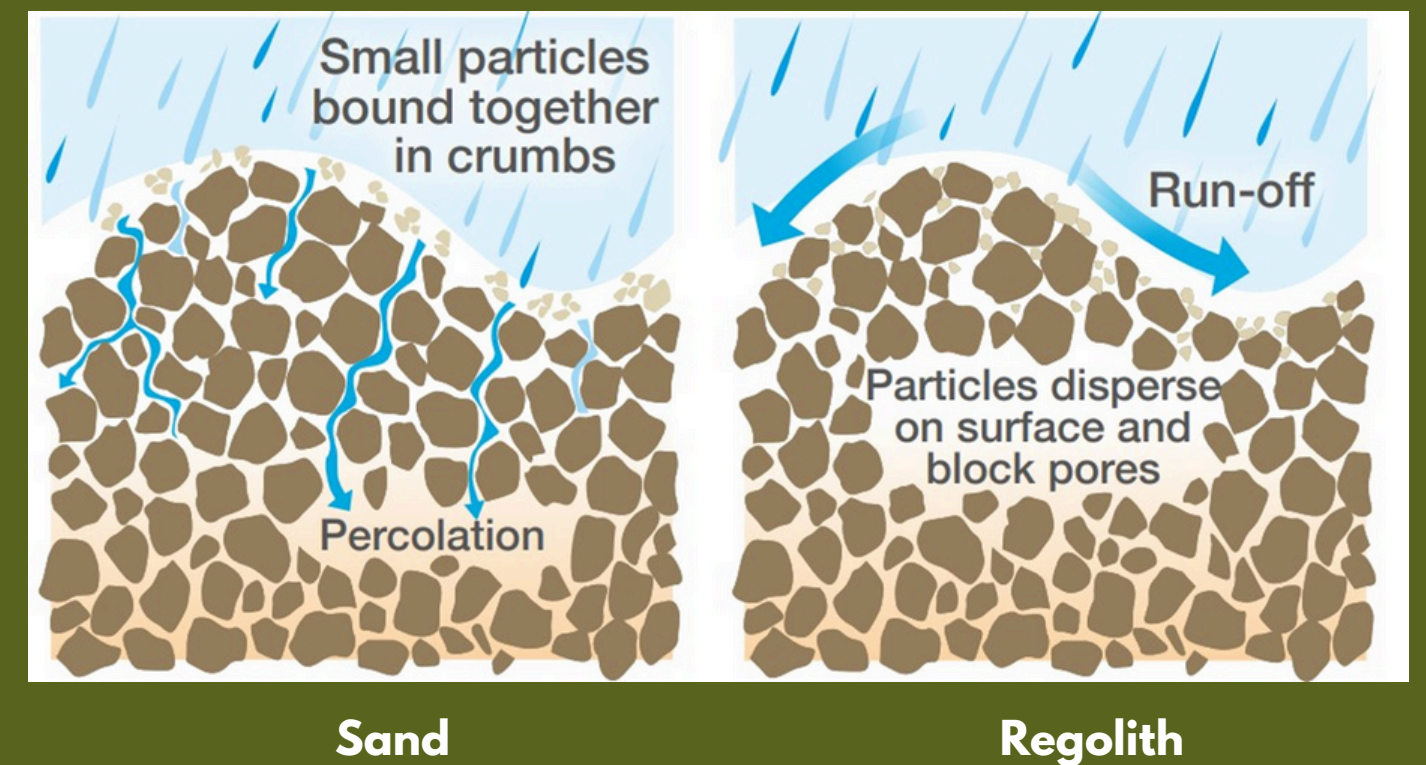
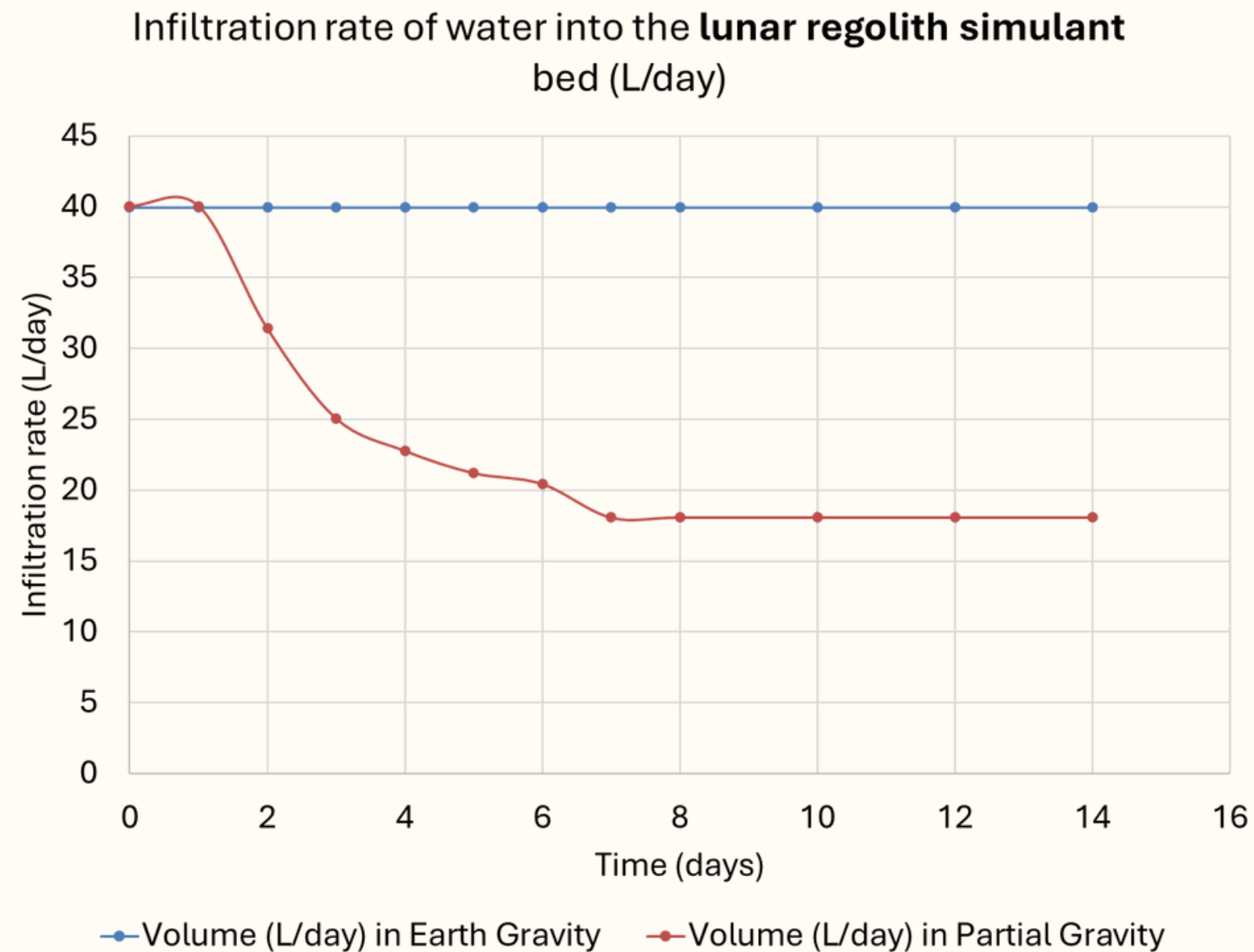
# Hydrodynamic Modelling - Configuration



2D modeling of variably saturated flow through porous bed



# Hydrodynamic Modelling - Infiltration

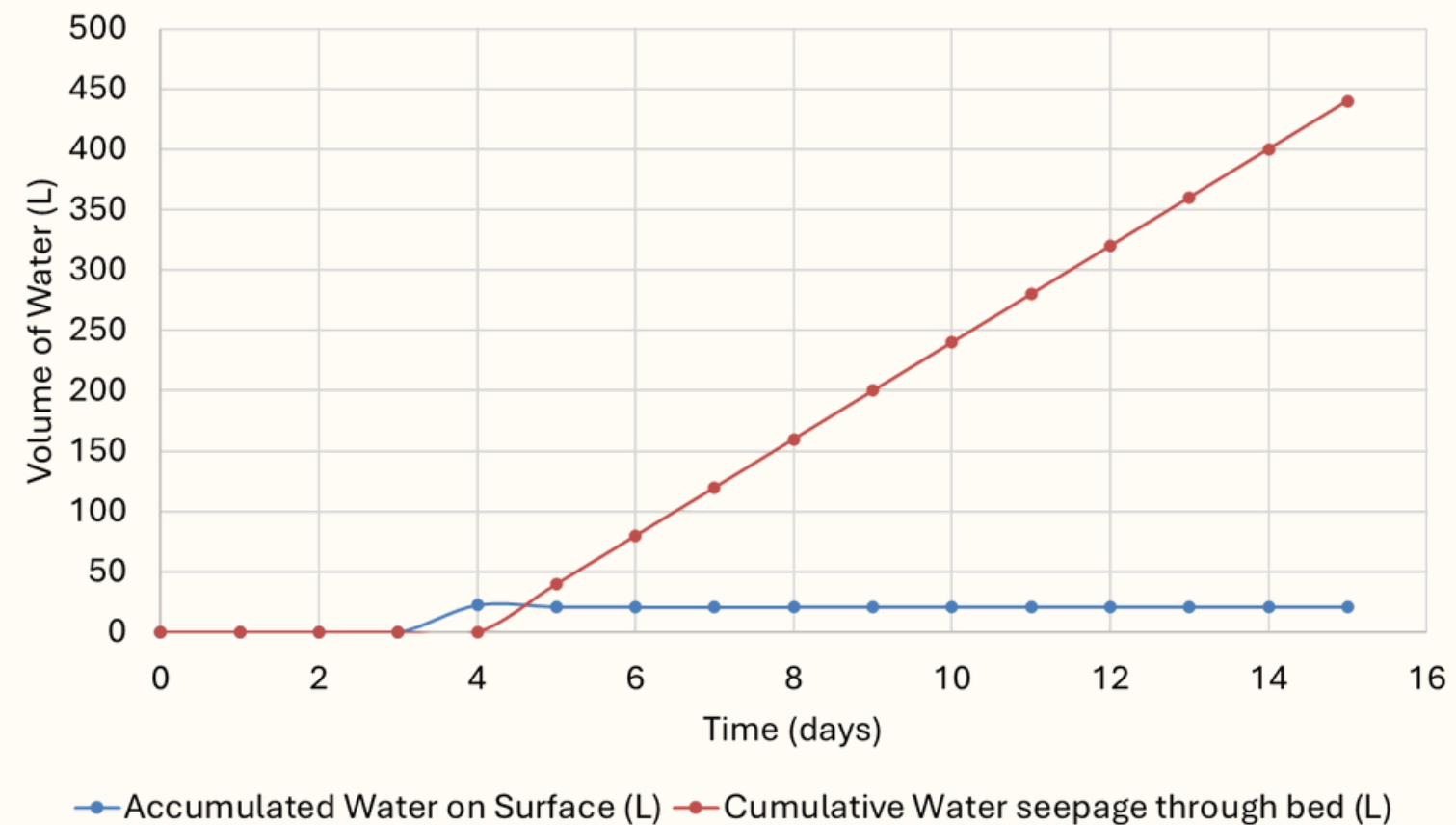


- **Reduced water infiltration rates over time in partial gravity conditions in lunar regolith simulant**
- **Not observed using sand**



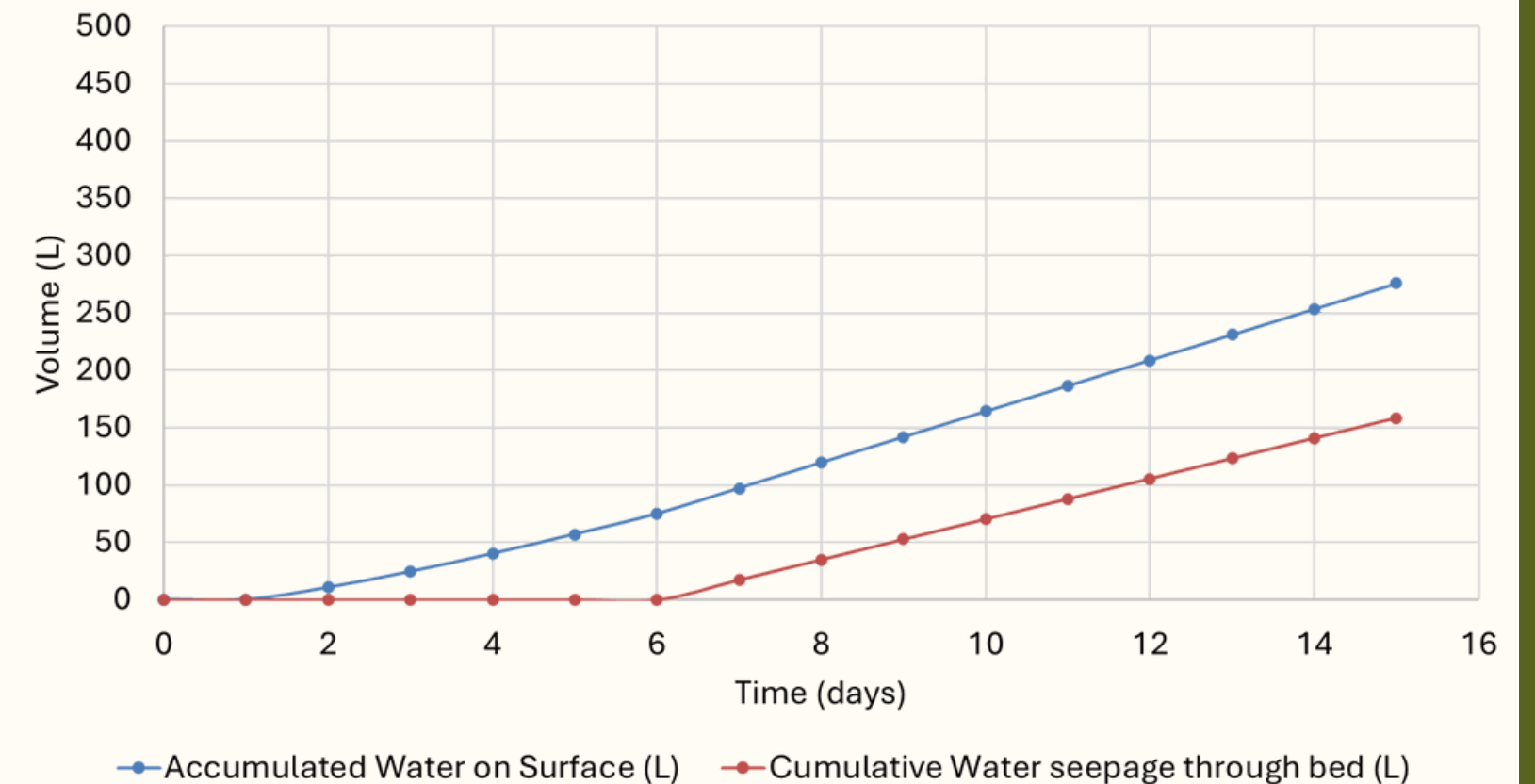
# Hydrodynamic Modelling - Runoff

Accumulation and seepage in lunar regolith simulant bed in  
**earth gravity**



**No increase in surface accumulation.**

Accumulation and seepage in lunar regolith simulant bed in  
**partial gravity**



**Accumulation faster than seepage causes  
runoff of untreated sewage. Gross!**



# Optimization of water dynamics in partial gravity using lunar regolith

Condition	Volume (L)	Feeding Time (hours)	Saturation time (days)	Surface runoff (L/day)
1	11.8	7.2	14	0
2	19.9	12	9.5	2.4
3	23.6	14.4	7.5	5.9
4	39.3	24	6	22.3
5	80	48	6	62.8

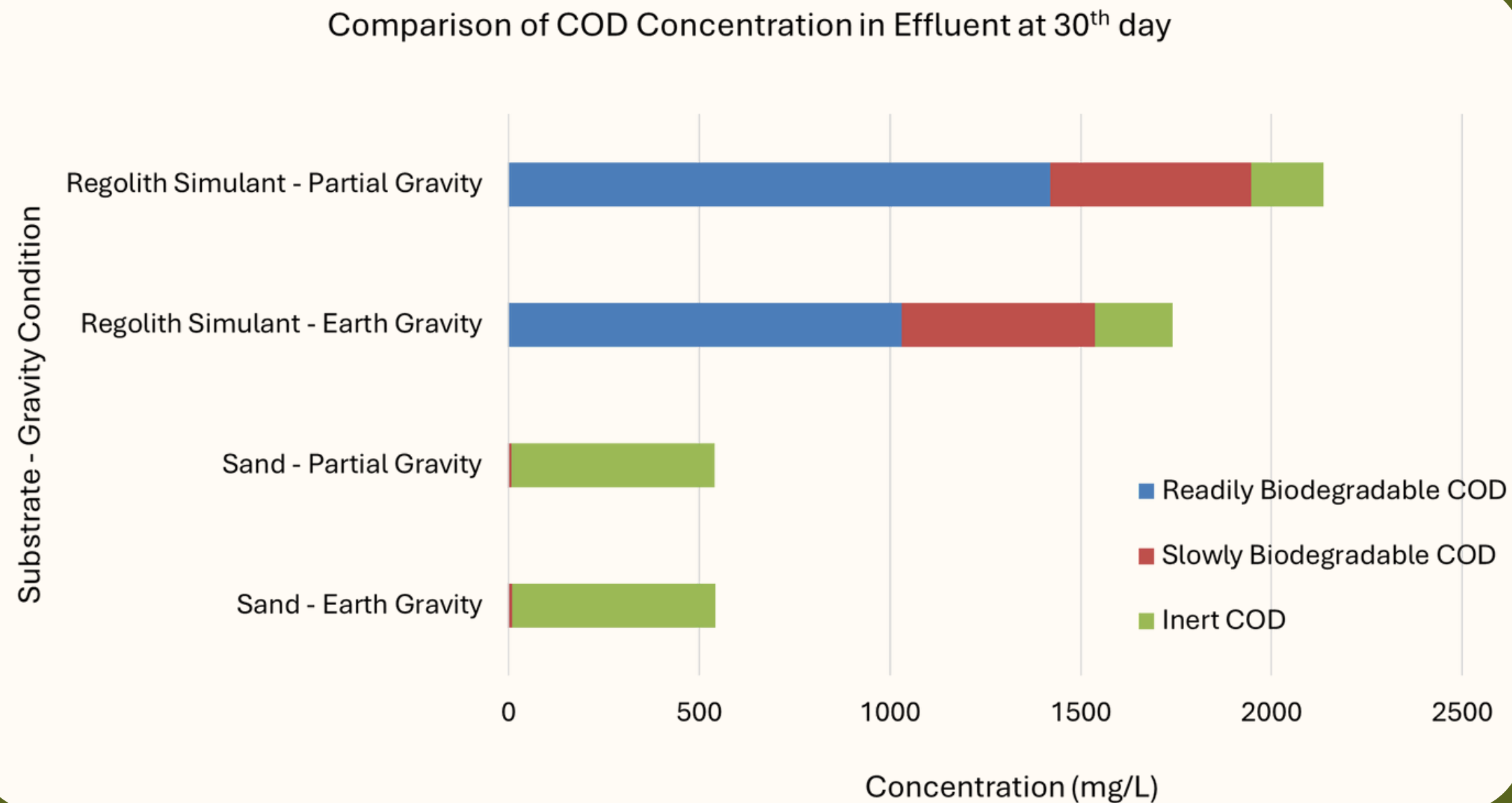
No surface runoff!

Solution found? Not quite.



# Contaminant Removal Modelling - COD Removal

Simulation results of contaminant removal in continuous feeding strategy ( $t < 1$  day)



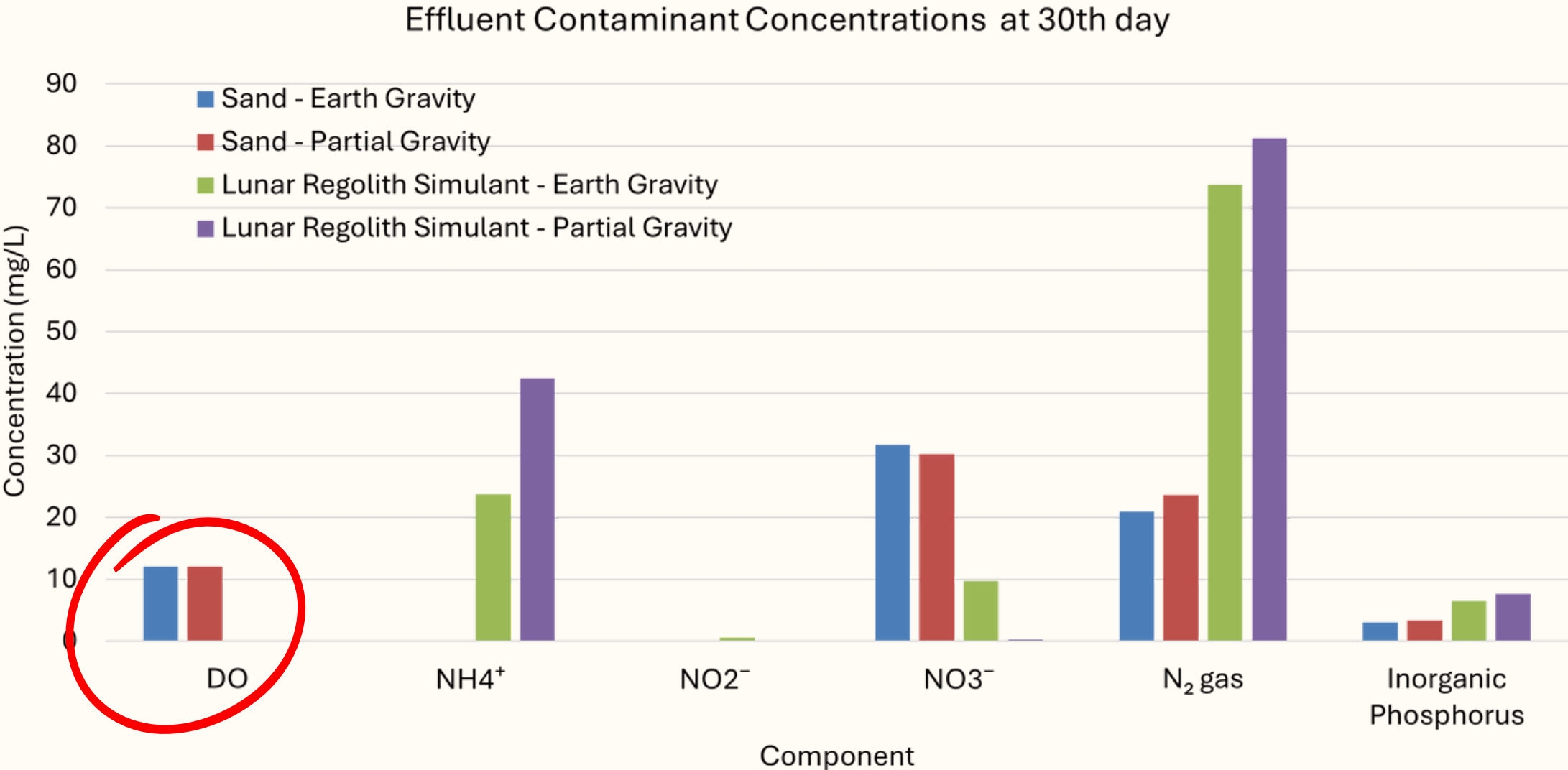
**Contaminant removal requirement not met in lunar regolith under any gravity!**

**Earth Sand works in all scenarios, though.**



# Contaminant Removal Modelling - Effluent Composition

Simulation results of contaminant removal in continuous feeding strategy ( $t < 1$  day)



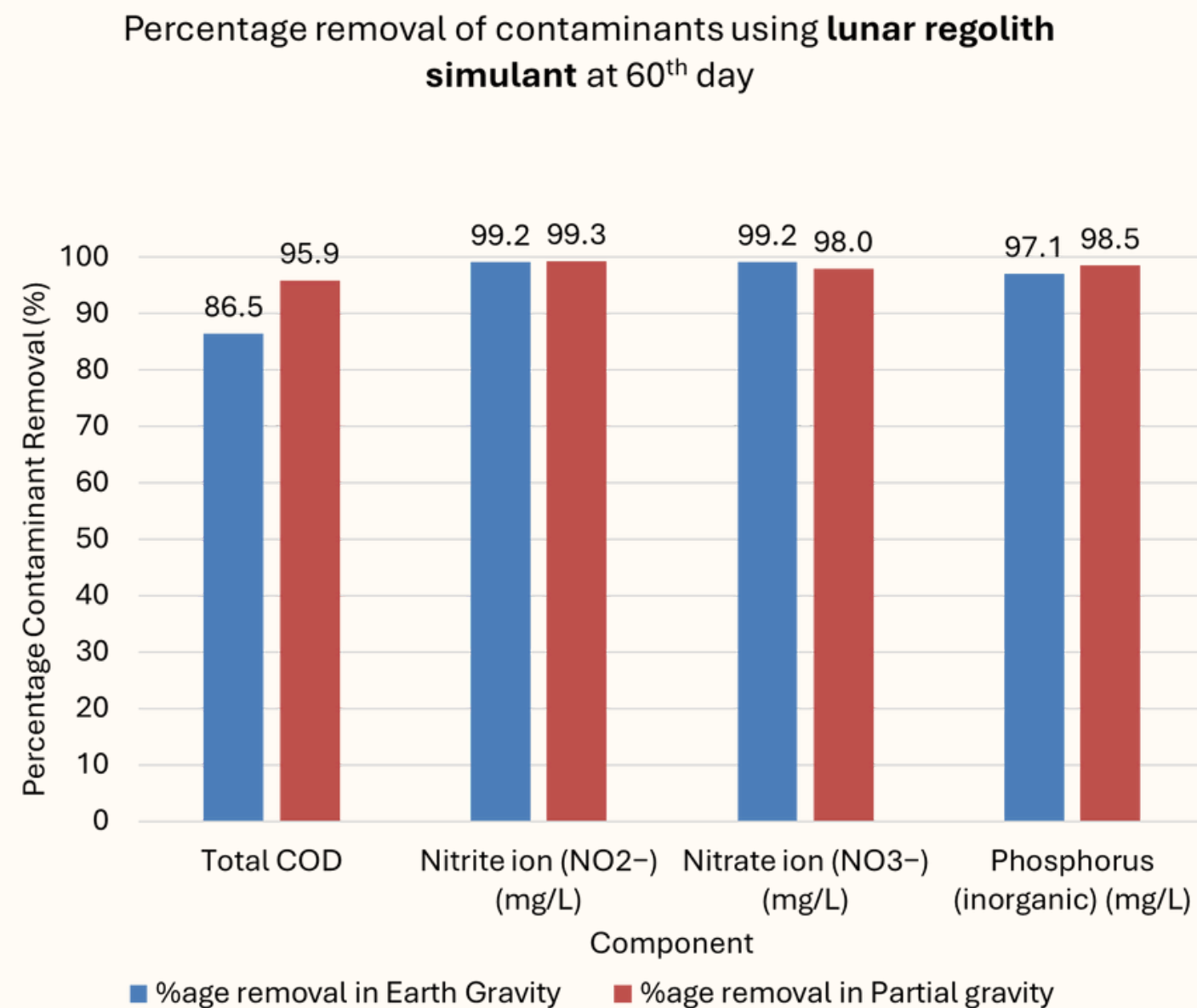
Lack of oxygen penetration into lunar regolith prevents aerobic metabolism (i.e. nitrification)

Components Modelled
Dissolved oxygen (DO)
Readily biodegradable COD
Slowly biodegradable COD
Inert COD
Ammonium ion (NH <sub>4</sub> <sup>+</sup> )
Nitrite ion (NO <sub>2</sub> <sup>-</sup> )
Nitrate ion (NO <sub>3</sub> <sup>-</sup> )
Dinitrogen gas (N <sub>2</sub> )
Inorganic phosphorus



# Contaminant Removal Modelling - Intermittent Feeding Alternative

Simulation results of contaminant removal in intermittent feeding strategy (t = 10 days)



- Higher COD removal compared to continuous strategy
- Increase the downtime of the system to 10 days
- Unfortunately also removes Nitrates and Phosphorus - still primarily anaerobic!

Meets treatment performance goal, but not daily load requirements.



# Conclusion

**CW offer effective lunar waste treatment using conventional sand.**

**Water movement is significantly slower in lunar G, but it helps improve microbial performance.**

**Lunar regolith as a wetland substrate is possible, but requires significant accommodations.**

**A CW can treat 4 astronauts' daily wastewater, though it would require support infrastructure.**

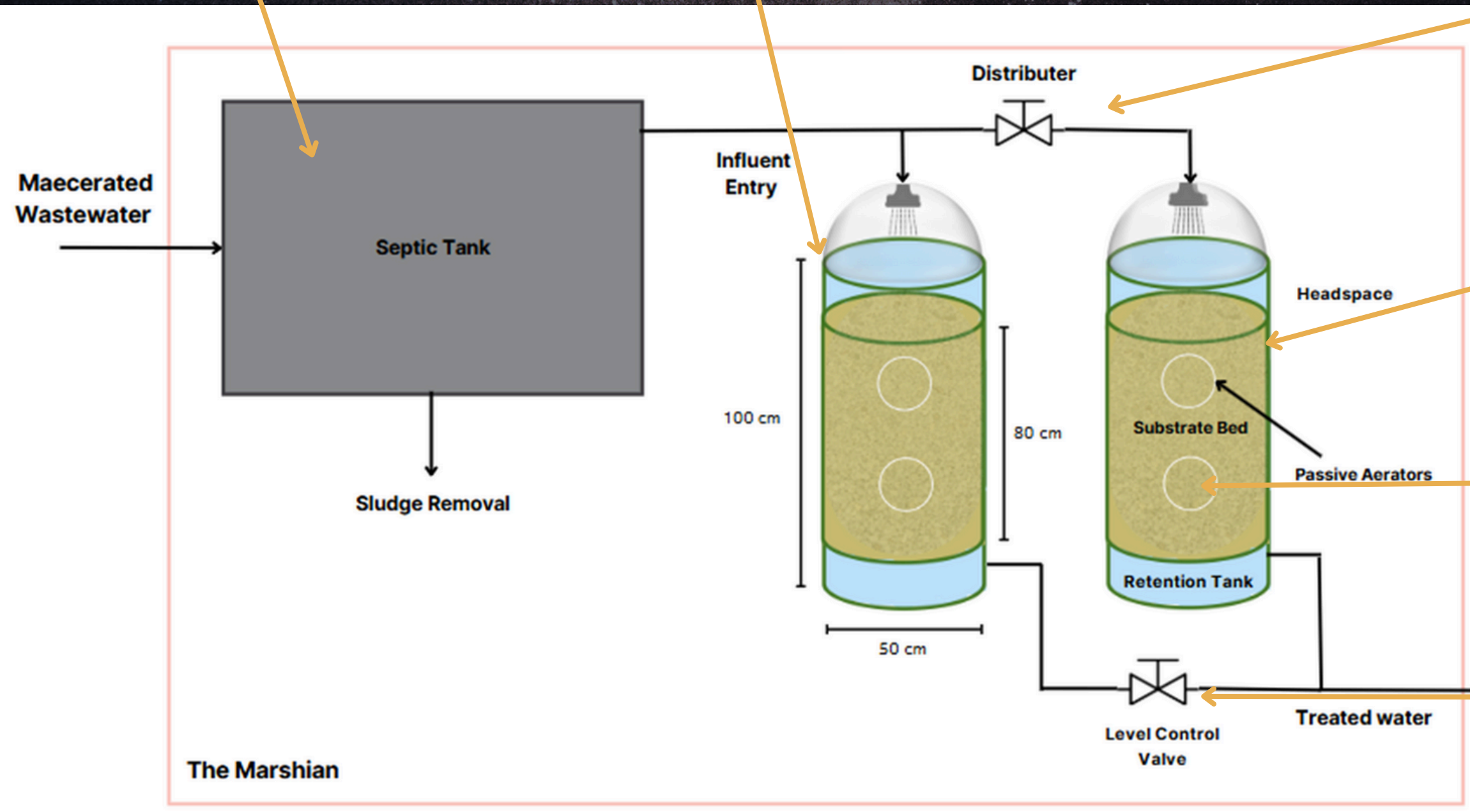


# Design and Operation Recommendations

Septic Tank halves initial COD

High freeboard to protect against surface accumulation

Parallel beds with alternating rest periods



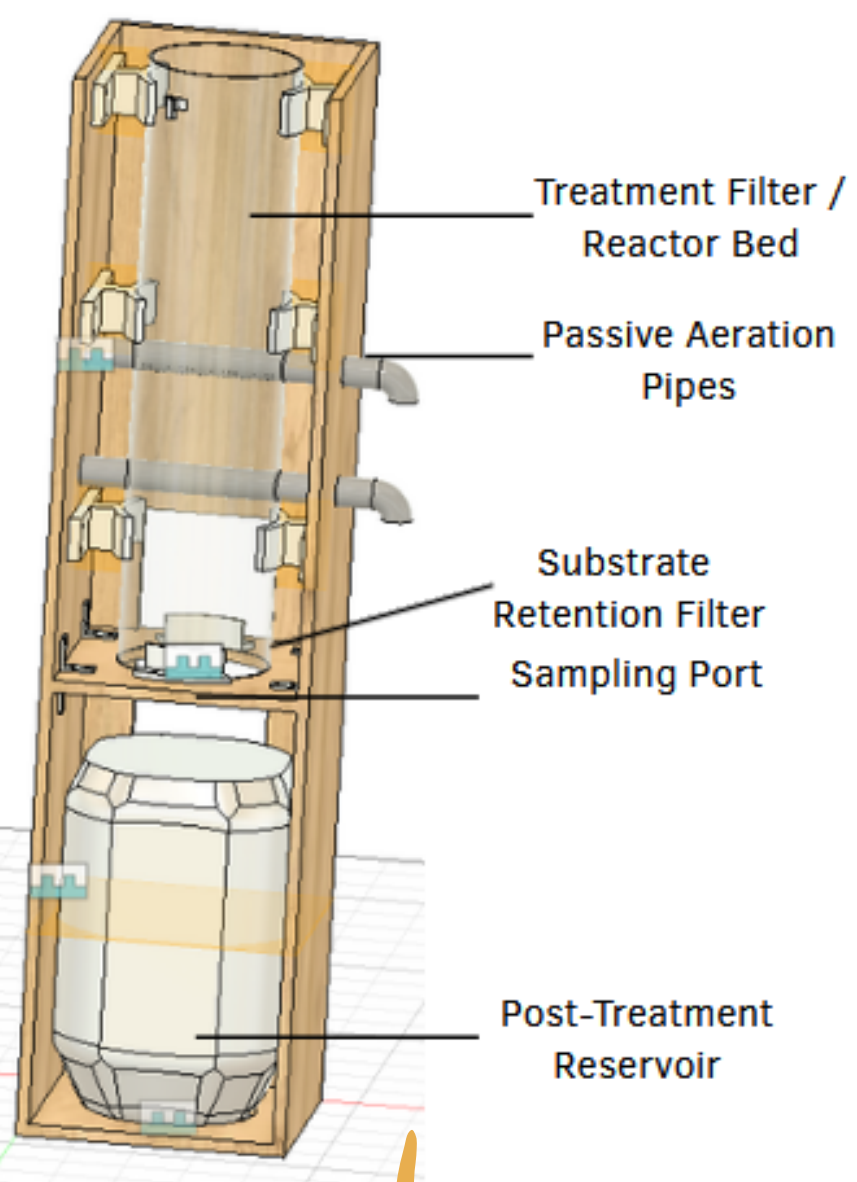
Sieve regolith to larger particle size (1-2mm)

Passive oxygen injection via pipes

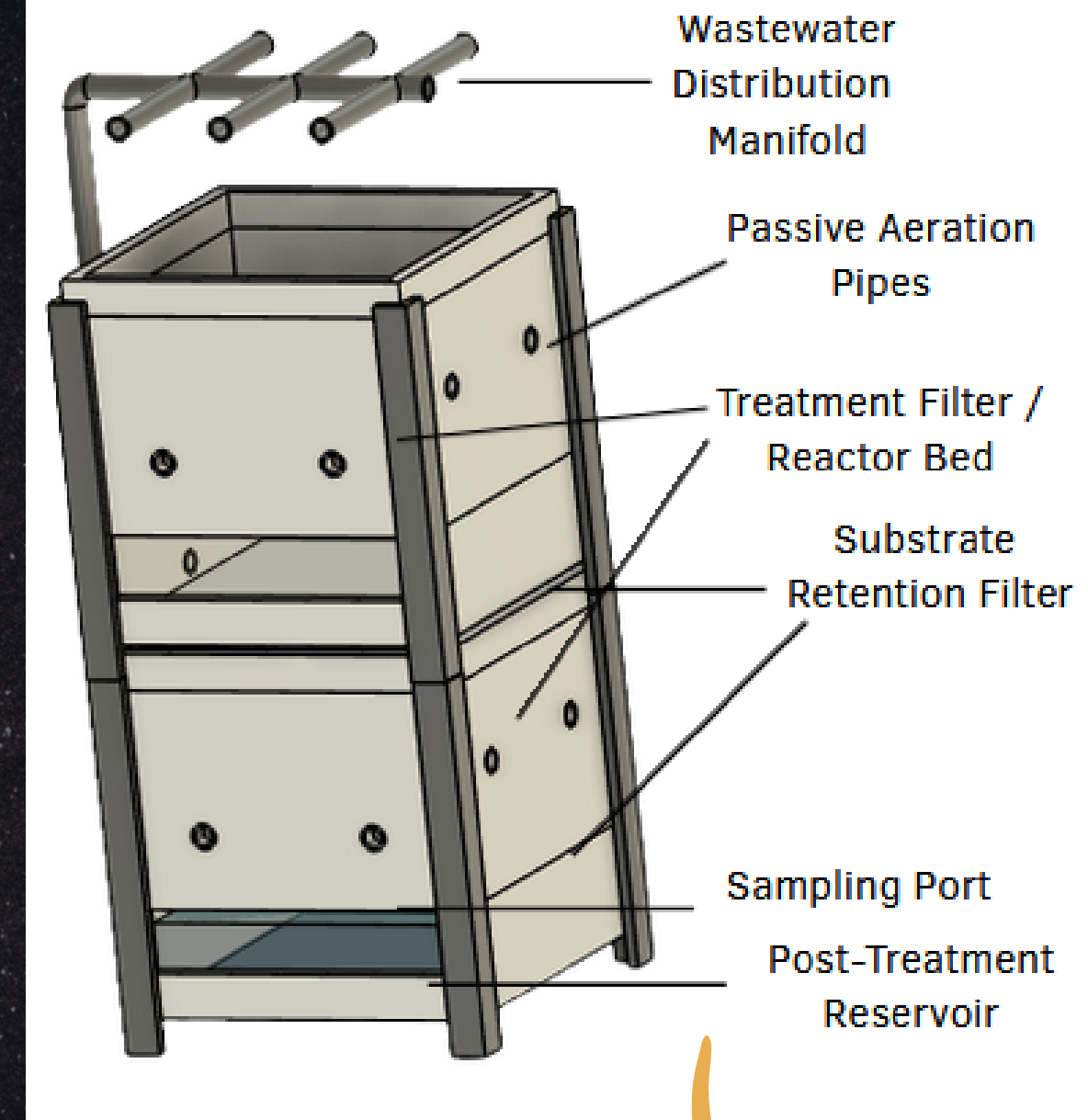
Process feedback control loop for automation of the system



# Current Status



**“Bench” scale prototypes  
for simulation validation**



**Full scale model TBD  
(To be deployed)**





# THANK YOU



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**CODY BAHAN**  
**ARTHUR CHARMASSON**



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# APPENDIX



# Simulation framework for water dynamics

- van Genuchten model for **hydraulic properties**
- Hydraulic parameters for lunar regolith simulant (LMS-1) have already been estimated

Parameter	Interpretation
<u><math>\theta_r</math></u> (Residual Water Content) [-]	Minimum water content left in the bed after drainage
<u><math>\theta_s</math></u> (Saturated Water Content) [-]	Maximum water content when the soil is fully saturated
$\alpha$ (Air Entry Suction Pressure) [1/cm]	Determines the pressure at which air enters the soil pores
$n$ (Pore-size Distribution Parameter) [-]	Describes how uniform the pore sizes are
$K_s$ (Saturated Hydraulic Conductivity) [cm/day]	The rate at which water moves through fully saturated soil
$l$ (Pore Connectivity Parameter) [-]	Empirical parameter influencing hydraulic conductivity under unsaturated conditions



# Simulation framework for water dynamics

Effect of reduced gravity

## Water dynamics through porous wetland bed in partial gravity conditions

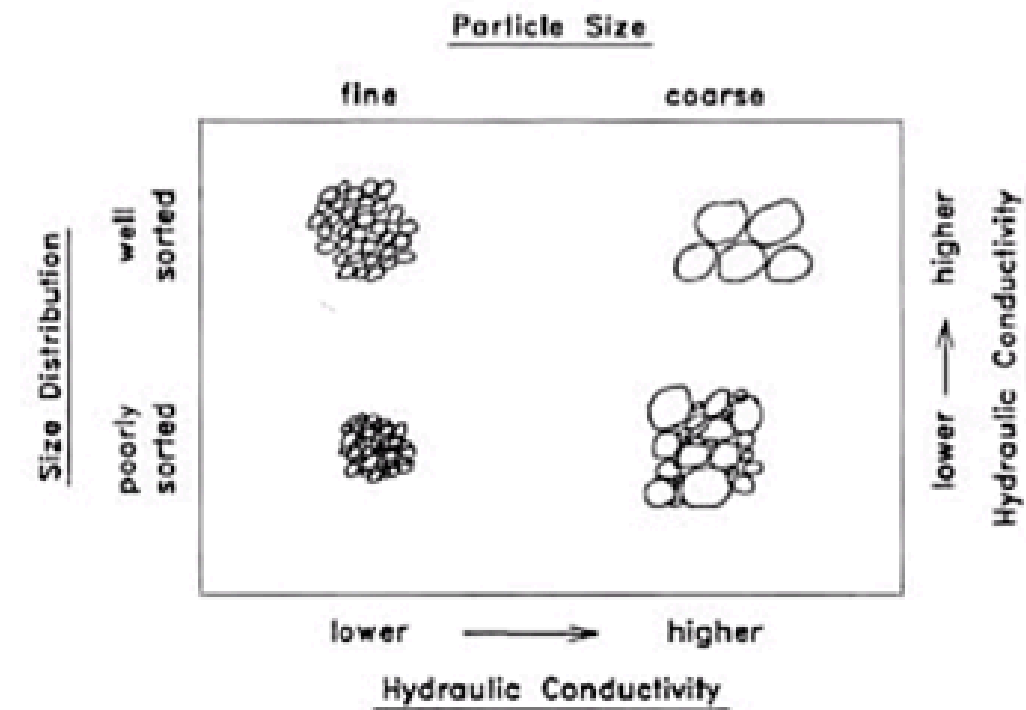
Richard's equation:

$$Q = -K(\theta)(\nabla h + \nabla z)$$

Total height =  $(\nabla h + \nabla z)$

Hydraulic conductivity =  $K(\theta)$

(Bonan et al., 2019)



### Estimation of hydraulic conductivity for partial gravity conditions

Using Karmen-Cozney's correlation for hydraulic conductivity:  $K_{sat} = k \left( \frac{\rho g}{\eta} \right)$

Where  $k$  is permeability ( $m^2$ ),  $g$  is gravitational acceleration ( $m/s^2$ ),  $\eta$  is dynamic viscosity ( $kg/ms$ ), and  $\rho$  is the liquid density ( $kg/m^3$ )

$g = 9.81 m/s^2$  for Earth

$g = 1.62 m/s^2$  for Moon

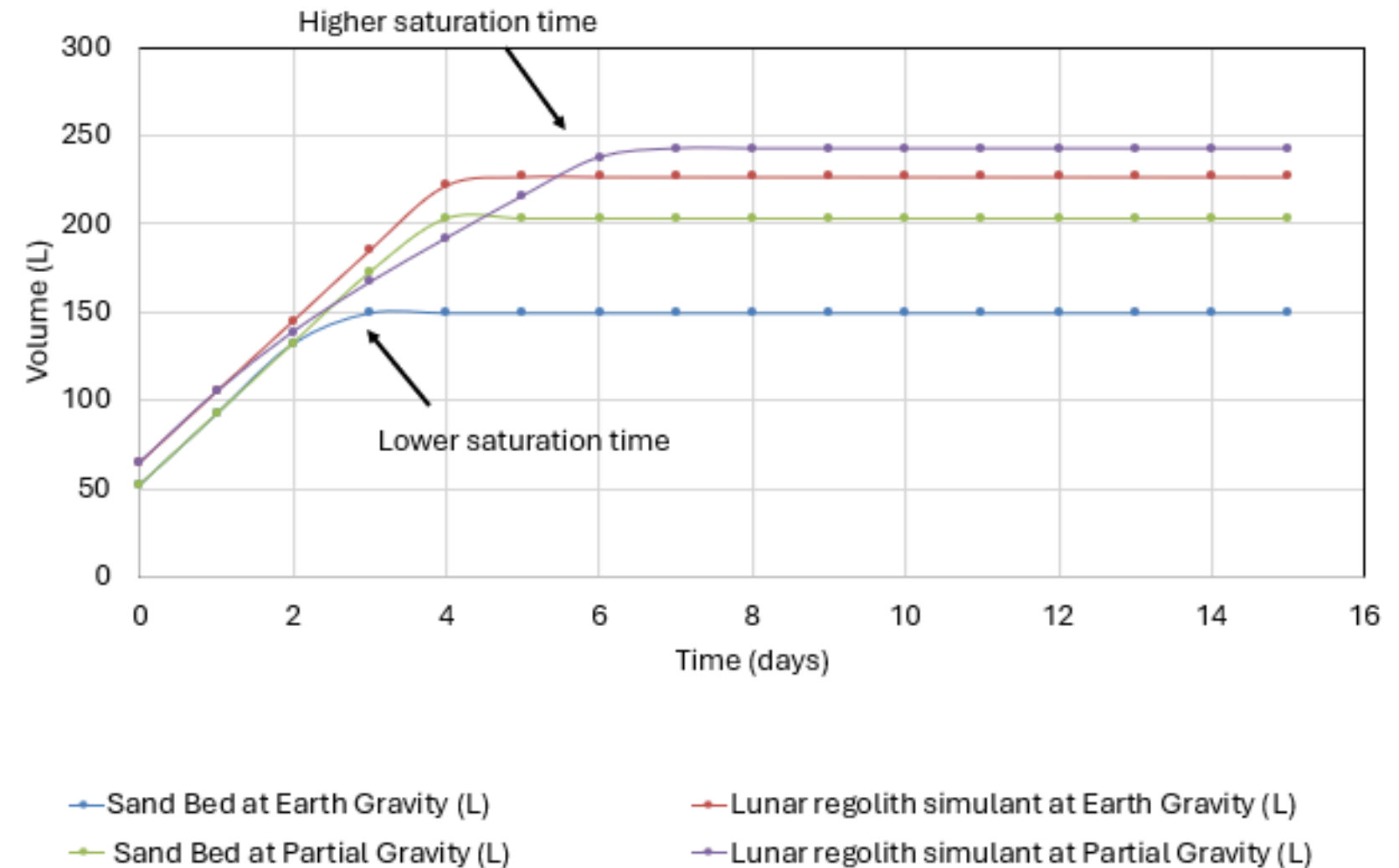


## Simulation results of water dynamics using 40 L/day

- Inherent difference in water storage capacity due to **substrate nature**
- Higher saturation time in partial gravity conditions

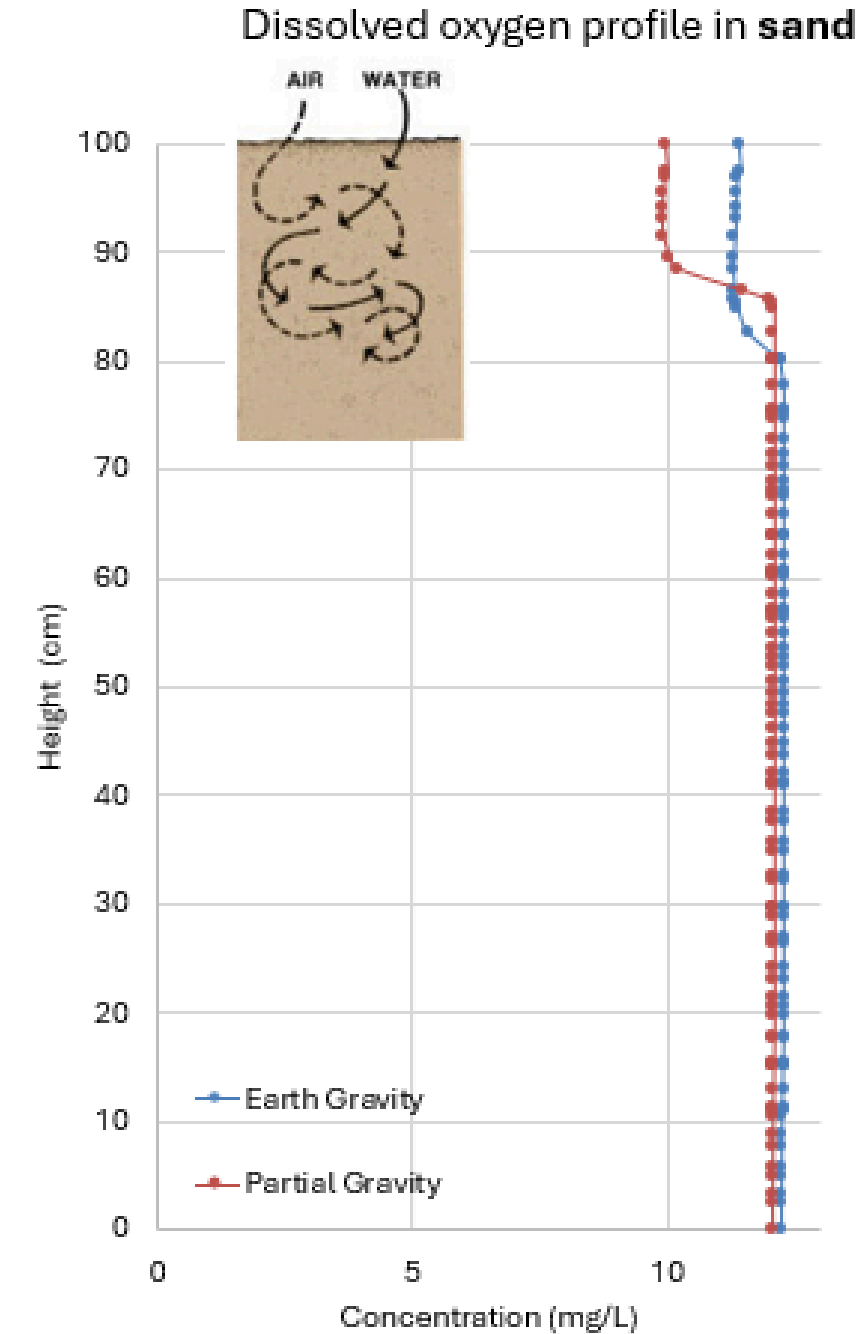
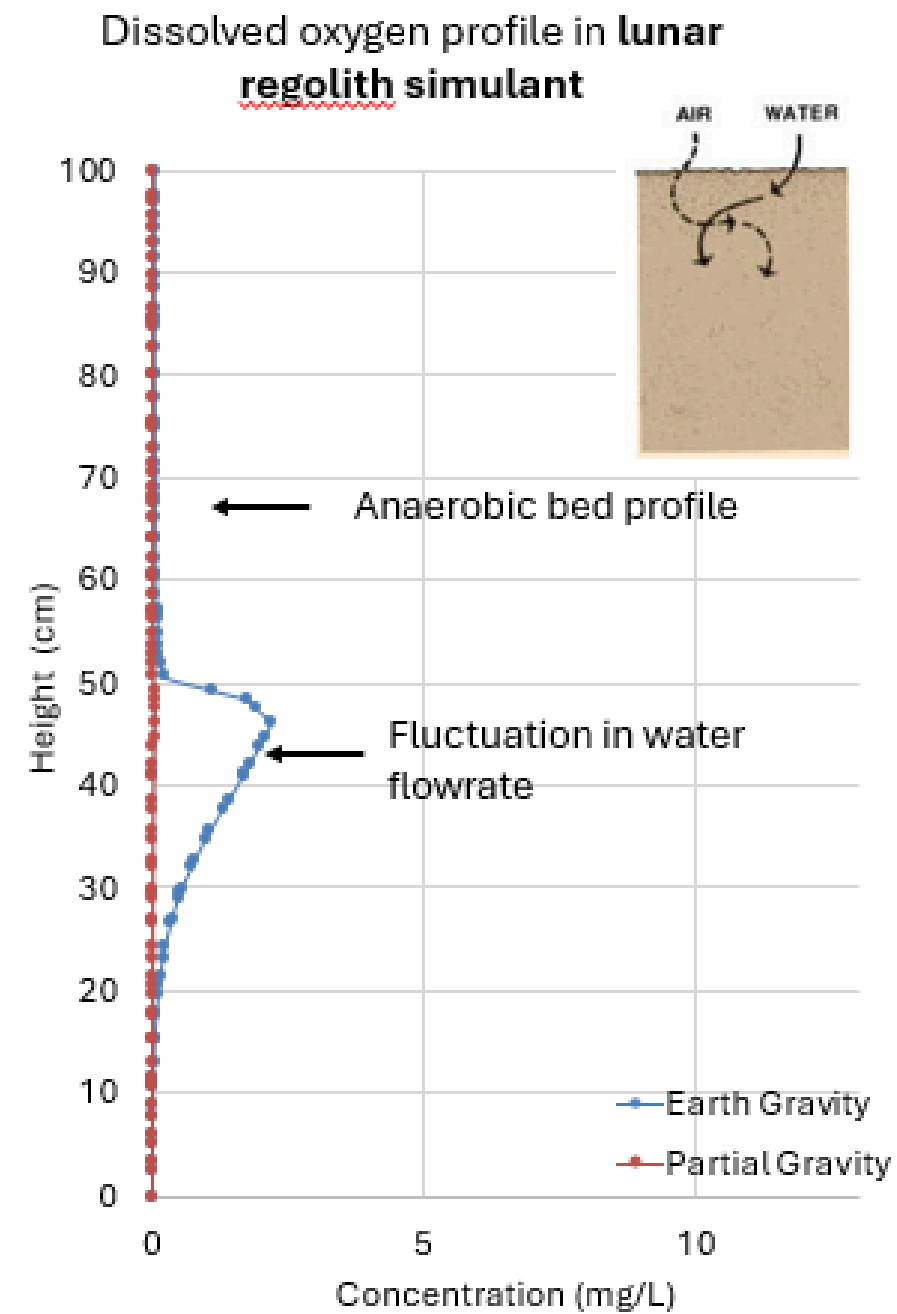


VFCW water storage capacity comparison for 40 L/day loading





## Simulation results of contaminant removal in continuous feeding ( $t < 1$ day)



### Possible Causes

- Higher entry suction pressure of lunar regolith simulant



